



The Society for Protective Coatings

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FEATURES



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SELECTING COATINGS FOR OFFSHORE WIND FARMS

By Anders Voldsgaard Clausen,
Hempel A/S

Offshore wind farms require high-performance coatings that can protect the structures for their entire service lives with minimal or no maintenance. This article is about new and innovative paint technologies being developed to deliver this requirement and enable facility owners to reliably protect their assets.



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WASTEWATER CLARIFIERS: UNDERSTANDING CORROSION MECHANISMS

By D. A. Sherman, P.E. and R. A. Nixon,
Corrosion Probe, Inc.

Wastewater treatment plant clarifier environments present challenges for selecting construction materials. Coated carbon steel, hot-dip galvanized steel and stainless steel are most commonly specified for new or refurbished clarifier mechanisms, and all have their advantages and disadvantages with regard to achieving the intended design life. This article discusses the corrosive conditions in primary and secondary clarifiers; how various process conditions can affect the corrosion mechanisms; in what situations each of these construction materials is or is not appropriate; and how fabrication quality and other details can affect corrosion resistance.



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2018 ANNUAL EQUIPMENT BUYING GUIDE

The JPCL Equipment Buying Guide lists products, equipment and supplies for protective and marine coating work from manufacturers, distributors and rental companies located around the world. As in previous years, the Equipment Buying Guide is based on surveys completed by equipment companies known to JPCL.

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SSPC Fills Leadership Posts, Announces Promotions

The growth trend at SSPC: The Society for Protective Coatings continues in 2018 as the organization recently announced several staff additions, promotions and key changes related to its May 15 reorganization.

Key additions include the hiring of Kevin LaRue as the new director of technical services, and Greg Muha as the new director of member development and engagement.

LaRue joins the SSPC staff after several years as vice president of the Finishing Contractors Association International based in Oakbrook Terrace, Illinois. Previous to FCA, LaRue was national director of the Labor Management Cooperation Initiative (LMCI) in Hanover, Maryland and national recruitment manager for Finishing Trades Institute. With his experience as a painting contractor as well as his background as an instructor and training provider, SSPC expects LaRue's transition to be seamless. At SSPC, he will work closely with staff and members on the development of SSPC standards and training programs, as well as oversee the PCCP (QP) programs.



Kevin LaRue

Muha comes to SSPC after 20 years at SAE International, where he served in many leadership roles, including his most recent as director, strategic partnerships and business development. With his experience in establishing and fostering business relationships, SSPC expects Muha's leadership to be a valuable asset in improving upon the customer experience. At SSPC he will work closely with staff and members on implementing new member benefits and programs to better represent SSPC's global reach.



Greg Muha

In addition to these new hires, Jennifer Merck has been promoted to the new position of director of training and certification. Having been with SSPC more than 18 years, Merck has been an integral player in the growth of SSPC's training and certification programs, as well as a key component in maintaining DoD-funded contracts for SSPC to train and certify more than 3,500 military personnel. As training courses developed and grew to host over 7,000 students per year with an average of 50 training and certification programs being offered every month, it became necessary for a new and independent department to focus on maintaining that growth.

Longtime SSPC directors Terry Sowers and Michael Damiano are moving into senior advisory roles. Sowers, who has been with SSPC since 1989 and plans to retire in 2019, will be working in the role of senior member services advisor, and Damiano, who has been with SSPC since 1991, will be the senior technical advisor and lead special projects.

Since 2006, Sowers has been the director of membership services, where she has improved upon delivery of SSPC training programs, quality of the technical program of the annual conference, as well as the core values of both individual and organizational membership. Her extensive history with SSPC and its member base are a testimony to her dedication to both the organization and its valued members. In her new role as senior member services advisor, Sowers will take on special projects in membership development, and will continue promoting SSPC chapter events. In addition, she will work as an advisor to Muha as he steps into his new position.

Damiano joined SSPC as the manager of the Painting Contractor Certification Program (PCCP) and contractor pre-qualification before being named manager of technical services in 1994 and director of product development in 1997. In 2015, he was named the director of technical services. Over the years, he has directed activities to develop and validate SSPC certification programs, standards, publications and training programs. He has been a key figure in the growth of the PCCP (QP) program and an important leader and historian among SSPC staff. In his new role as senior technical advisor, he will take on special projects in training and program development, and will continue representing SSPC at meetings and events. In addition, he will work as an advisor to LaRue in his new position.

Other promotions announced by SSPC include Sara Badami assuming the role of training manager and Dustin Young taking on the role of training materials development manager.

Badami has been directly involved with SSPC's training and certification programs for the past 14 years. Under her leadership, the training staff has been better equipped to process the increase in programs being offered, all while maintaining a quality product and responsive customer service. Her managerial duties will include the growth of international training licensees as well as the promotion of SSPC training and certification programs domestic and abroad.

Young joined SSPC as a technical service specialist in May 2017. He has worked in and around the coatings industry since 2011, previously holding positions with Ferro Corp., a glass coatings manufacturer, and PPG Industries. In his new role, Dustin will oversee the development and revision of all SSPC training and individual certification materials to stay current with industry updates and trends.

SC Bridge Reopens After Corrosion-Related Cable Failure

The James B. Edwards Bridge in Charleston, South Carolina, re-opened June 2 after more than two weeks of work stemming from what officials now say was a cable failure caused by corrosion.

The bridge, which carries Interstate 526 over the Wando River, was closed by the South Carolina Department of Transportation on May 14 after a routine inspection uncovered a severed cable inside the westbound span of the twin-span concrete box-girder bridge. It was the second time in less than two years that a cable was found to have been damaged inside the structure.

SCDOT had a new cable installed to replace the damaged one, and fabricated and installed an additional cable for the sake of redundancy in case of any future cable



Photo: www.twitter.com/SCDOTPress

problems. Officials had previously predicted the bridge would reopen June 11; the repair beat that time estimate by more than a week.

SCDOT said that an investigation had determined that corrosion caused by moisture intrusion had caused the cable failure,

and that corrosion had also been to blame for the failure of another cable in the same span in 2016.

Moisture intrusion has been a known issue on the bridge since long before the 2016 incident. In 2011, a paper authored by a group of Clemson University engineers used the bridge as a case study, noting that SCDOT had identified problems including “improper grouting of ducts, leaky joints, debris in the box void, clogged drain holes [3/4-inch-diameter] and cracks in the piers.”

The agency says testing was performed last year on seven of the main cables in the westbound span — not including the one installed just last year — but results are still pending in that investigation. “Preliminary information” indicates corrosion areas were found on two of the cables, the agency says.

G.C. Zarnas Celebrates 70 Years

For the nationwide industrial and commercial coatings contractor G.C. Zarnas & Co., Inc., this year marks a significant milestone: the 70th year since the Bethlehem, Pa.-based company's founding in 1948.

G.C. Zarnas Vice President Dean Zarnas attributes the longevity and success of the company today all the way back to the company's founder, his grandfather, Gust C. Zarnas — a Greek immigrant and child of the Great Depression who became an All-American football player at Ohio State University and spent three years in the NFL before returning home and eventually entering the steel painting business.

Gust's father, who was then a paint superintendent at the nearby Allegheny Steel Mill, convinced Gust to get into the business himself, and in 1948, Gust started G.C. Zarnas after securing the then-booming Bethlehem Steel as the company's first client. Coincidentally enough, the purchasing agent at Bethlehem Steel was an Ohio State graduate who had keenly watched Gust's athletic exploits on the field back in Columbus, says Dean.

Though early operations ran out of the company's sole vehicle — a 1938 Ford truck, which Dean says the family keeps to this day — steady and successful jobs at Bethlehem Steel opened the door to work at other mills in Maryland, New York and Indiana. Gust's son Stephen was instrumental in developing partnerships beyond Bethlehem Steel with chemical and petrochemical giants and several power generation plants.

As the years went by, the company evolved from strictly

performing maintenance to incorporating new construction projects, including commercial facilities such as arenas and hotels. In addition to surface prep and coating application, the company added lead abatement, fireproofing and other specialty services to its repertoire. This diversification of services proved crucial when the U.S. steel industry faltered in the 1970s and 1980s, as the company shifted work into other industry sectors.

Nowadays, G.C. Zarnas continues to operate in these arenas, all while adhering to developing standards, regulations and trends in the industry. Dean says the company has raised its quality standards to reflect these developments, earning SSPC-QP 1, 2 and 8 designations, as well as SSPC-QS 1 and NACE certifications.

As for the next 70 years, Dean, his brother, Lee, also a vice president; and their father, Stephen, company owner and president; hope for what Dean calls “sustained, modest growth.”

“We don't strive to be the biggest company,” says Dean. “We want to serve our existing customers well, while partnering with new clients that align with our high-quality standards.”

And while Dean can point to a number of noteworthy projects the company has taken up over the past 70 years, the true highlight to him is the positive impact the company has had on its employees lives — to which Dean ultimately credits his grandfather.

“For him to earn a scholarship, get a degree, become a star athlete, start a company and create a livelihood for so many — that says a lot,” says Dean. “It's a huge testament to his motivation.”



PAINTSQUARE COMMENTS

In Response to "Pentagon Concerned About Gulf Offshore Expansion"

(PaintSquare News, May 14)

The Pentagon said in a recent report to Congress that offshore drilling in the eastern Gulf of Mexico would cause problems for necessary military activities carried out in the region, and that any drilling conducted there would have to be placed under significant restrictions to prevent interference with military operations. That portion of the Gulf was deemed an "irreplaceable national asset," according to reports.

Robert Bullard:

"This same situation may [relate] to the development offshore wind power development, especially as the industry matures to deeper-and-deeper-water operations."

David Knuckey:

"Why can't the Administration and the DoD get together and discuss these issues before going public? It really makes us look inept in the eyes of the world when things like this happen."



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Paint Poll

paintsquare.com/poll

The U.S. military has expressed recently that it would like to block offshore drilling and wind projects in some U.S. waters where it operates. Should military exercises trump energy development at sea?

Maybe, but military exercises should be only one of the factors considered in permitting offshore development. 53%

Yes. Military security is crucial. 43%

No. Domestic energy development is important, and military exercises can be moved. 4%

Problem Solving Forum

How do you best remove lubricants and other contaminants from field-bolted connections prior to painting?

Jonathan Pavlik, PBI Custom Finishes:

"Remove the material in accordance with SSPC-SP 1, if specified. Water-soluble, environmentally friendly alkaline cleaners combined with elbow grease can provide a water-break-free surface suitable for surface-tolerant coatings."



Trevor Neale, TF Warren Group:

"Hundreds or thousands of field and/or shop bolt assemblies that require full corrosion protection can be found on bolted structures. SSPC-SP 1 is the minimum standard, but in some cases where galvanizing was specified, a special primer or treatment may be required and is rarely detailed in the specifications. This is a good example of the type of item to be discussed at the pre-job meeting."

PAINTSQUARE NEWS TOP 10

paintsquare.com/news, May 6–June 3

1. Steel Used on \$1.6B Subway Project Questioned
2. Hempel Acquires Majority of German Paint Firm
3. SC Bridge Closed After Cable Breaks
4. Report: FIU Bridge Showed Cracking 10 Days Before Collapse
5. Gordie Howe Progresses as Contractor Withdraws
6. Pentagon Concerned About Gulf Offshore Expansion
7. PPG Fires Controller Amid Accounting Investigation
8. Dubai Starts \$107M Bridge Project
9. Report: Worker Fled FIU Bridge Collapse
10. SC Bridge with Snapped Cable Closed for 4 Weeks

Delamination of Coating from a Ship's Hull

BY CHERYL ROBERTS, KTA-TATOR, INC.

Unlike many industrial structures, ships often contain a variety of multi-layer coating systems on a single vessel, and even on the exterior hull itself, often including a complex sequence of anticorrosive layers followed by antifouling layers. This article focuses on the recoating of a ship's exterior hull that resulted in catastrophic failure before the ship was ever returned to service.

THE BACKGROUND

The exterior hull coating on a large ship was installed about 25 years after its initial launch. Specifications required blast cleaning to SSPC-SP10/NACE No. 2, "Near-White Blast Cleaning." The hull was divided into three segments with each coating layer applied in a different color (Fig. 1).

The underwater hull was to be coated with two layers (red, then gray) of an anticorrosive (AC) polyamide/polyamidoamine-cured epoxy at 4-to-8 mils DFT followed by three layers (red, black, then red) of an antifouling (AF) polyamide cuprous oxide coating at 4-to-6 mils DFT.

The boot top was to be coated with two layers (red, then gray) of the AC coating at 4-to-8 mils DFT followed by three layers of the AF coating (red, then two coats of black) at 4-to-6 mils DFT. This layer of the hull is sometimes above the waterline and sometimes under water, depending on weight. The light-load line (LLL) is considered to be 6 inches above the

underwater hull and the deep-load line (DLL) 6 inches below the freeboard.

The freeboard (above the waterline) was to be coated with two layers (red, then gray) of the AC coating at 4-to-8 mils DFT, followed by a topcoat of amine-cured polysiloxane (gray) at 5-to-8 mils DFT to provide UV resistance.

After the coating work was completed, the ship was removed from the dry-dock and secured to a pier in the shipyard. Shortly afterwards, spontaneous peeling of the AF coating system from the AC coating was observed at various locations of the boot top around the perimeter of the ship. The peeling was most prevalent in an area from the DLL down approximately 3-to-4 feet around the perimeter of the ship. The AC coating beneath was intact and no rusting or deterioration of the AC was evident at any location.

Additionally, delamination of the coating was observed on the freeboard in an area from the top of the boot top up approximately 1-to-2 feet. This area was to have been coated with only the AC epoxy system and polysiloxane; however, there appeared to be an extraneous coat of the AF coating applied between the epoxy and polysiloxane. Two feet above the DLL, this same coating system showed no delamination, peeling or other notable defects.

FIELD INVESTIGATION

Samples were obtained from three locations within each area: a "lower" sample of the AF coating at or below the DLL and the intact AC coating beneath where the AF coating had been removed; a "middle" sample of any disbonded coating immediately above the DLL

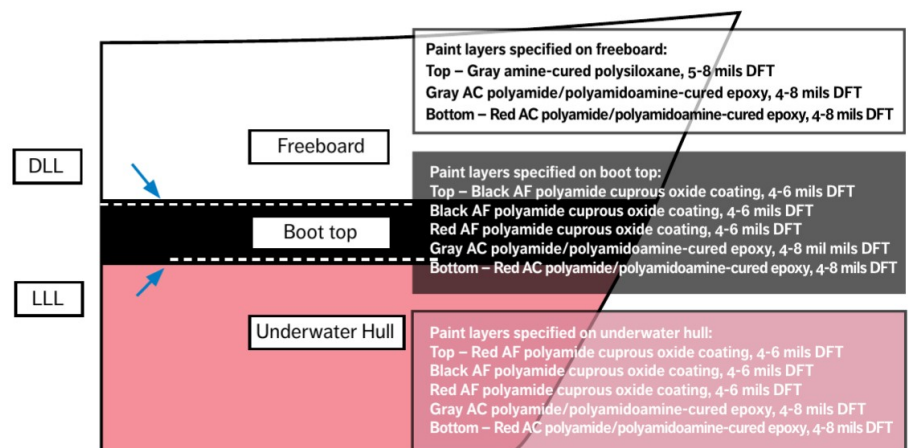


Fig. 1: An illustration of the hull of the ship with the deep-load line (DLL), light-load line (LLL) and specifications for the coating systems applied. Figures courtesy of the author.

INVESTIGATING FAILURE



Fig. 2: Lower, middle and upper sampling sites. The black area is the boot top.

and the AC coating beneath the disbonded coating; and an "upper" sample of the free-board polysiloxane. Figure 2 depicts the lower, middle and upper sampling locations.

In every case, upper samples of the free-board polysiloxane coating were tightly adherent with no loss of adhesion between coats or to the underlying substrate. The AC coating beneath any disbonded AF or polysiloxane coating was also tightly adhered with no loss of adhesion between AC coats or to the underlying substrate.

The adhesion of the AF coating to the underlying AC coating was somewhat variable,

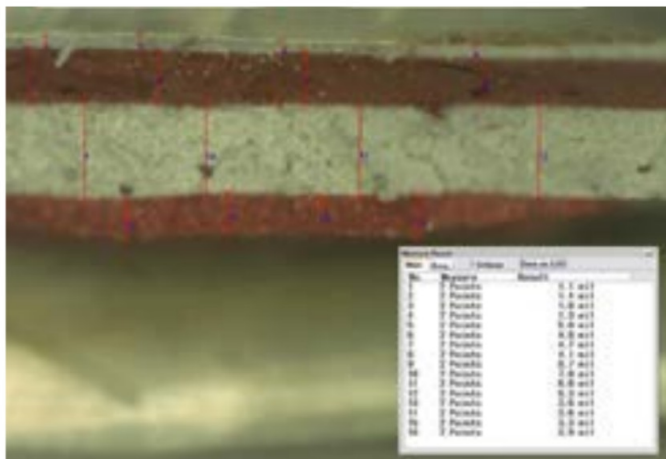


Fig. 3: Cross section of a paint chip obtained from within 1-½ feet above the DLL showing the extra red layer sandwiched between the gray layers at 200-times magnification.

ranging from tightly adherent to relatively poor. There were large areas where the AF coating could be easily and cleanly separated from the underlying AC coating by cutting or scraping.

LABORATORY INVESTIGATION

The laboratory investigation focused on obtaining answers to two questions: 1) why did the red AF coating disbond from the gray AC coating over a large portion of the ship, and 2) why did the gray polysiloxane coating disbond in the middle area extending from the top of the boot top to approximately 1-to-1½ feet above the DLL? The investigation consisted

of microscopic examination, mix-ratio analysis by nitrogen content and infrared spectroscopy (IR), a recoat interval study, comparative batch composition testing, an analysis for the presence of an amine exudate (blush) and a solvent rub test.

Microscopic Examination

Cross-sectional microscopy of the samples collected during the field investigation revealed that the thickness of the gray AC coating ranged from 5.4-to-8.9 mils; the thickness of the red AF coating ranged from 3.2-to-7.7 mils.

The examination of coating chips from the middle area extending from the top of the boot top to approximately 1-to-1½ feet above the DLL revealed an additional red coating layer between the gray intermediate coat and gray topcoat. A photomicrograph of one such coating chip is shown in Figure 3.

Solvent Rub Test

A methyl ethyl ketone (MEK) rub test was used as a qualitative method to determine what coating was present on the backsides of the chips. Because it was known that the AF coating readily dissolved in MEK but the red AC epoxy primer did not, it was concluded that disbonding occurred within the AF layer.

Nitrogen Analysis: Mix Ratio

Nitrogen content analysis of the gray AC coating was performed to assess the mix ratio of the epoxy components. According to the

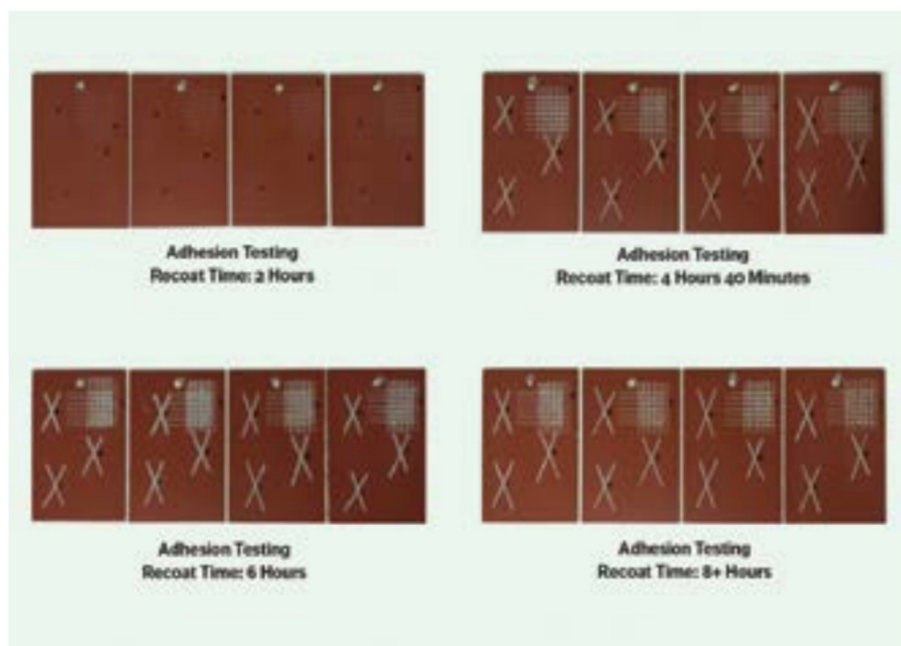


Fig. 4: Variations of adhesion with length of time between application of red AF and gray AC coating.

Table 1: Results of Tack-Free Study.

Ratio of A to B	Substrate/Surface Preparation/ Application	Time from AC Application until No Longer Wet	Time from AC Application until No Longer Tacky
1 : 1	Same as Recoat Study (Steel panel/ Abrasive blast/ Airless spray)	1 hour and 45 minutes	4 hours and 15 minutes
1.4 : 1	Same as Recoat Study (Steel panel/ Abrasive blast/ Airless spray)	2 hours	3 hours
1 : 1	Glass panel/ Cleaned with solvent/ Drawdown	1 hour and 45 minutes	4 hours and 15 minutes
1.05 : 1	Glass panel/ Cleaned with solvent/ Drawdown	1 hour and 45 minutes	4 hours
1.1 : 1	Glass panel/ Cleaned with solvent/ Drawdown	1 hour and 45 minutes	4 hours
1.4 : 1	Glass panel/ Cleaned with solvent/ Drawdown	1 hour and 30 minutes	3 hours

product data sheet, Part A of the gray AC coating contained polyamide and polyamidoamine, both of which contain nitrogen. The Part B component consisted of an epoxy resin. The analysis revealed that two of the seven gray AC paint chip samples had a proper 1:1 mix ratio, and that the other five samples tested had excess nitrogen, with mix ratios ranging from 1.05:1 to as high as 2:1. The infrared spectroscopic analysis was also performed but did not provide any further information.

Recoat Interval Study

A study of the relationship between the application recoat interval and the adhesion of the red AF coating applied over the gray AC coating revealed that a two-hour recoat interval produced markedly better adhesion than did longer recoat intervals. The adhesion test involved making "X" cross-cut incisions through the coating layers of prepared and coated test panels, applying tape over the incisions and then removing the tape. The degree of

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adhesion was evaluated based on how much coating was removed by the tape. Figure 4 (p. 10) shows the coated panels after the testing was complete.

Tackiness/Tack-Free Test

The time of tackiness was defined as the interval between when the coating was no longer wet (when paint ceased to transfer to a fingertip that lightly touched the surface) and when the coating was no longer tacky. The coating was considered no longer tacky when a light touch to the surface ceased to leave an impression on the surface.

The results of the tackiness/tack-free study established that at 80 F air temperature and 65-percent relative humidity (RH), the proper I:I mixed gray AC coating had a tack window of 2.5 hours (Table I, p. 11). Mix ratios of I.05:I and I.1:I had a tack window of 2.25 hours; and a mix ratio of I.4:I had a tack window of I-to-I.5 hours.

Batch Composition Testing

Paint retained from the original application was compared to control samples provided by the coating manufacturer, and compositional values were found to be reasonably consistent. Unfortunately, original samples of the red AF coating and the Part A component of the gray AC coating were not available for testing.

Amine Exudate Analysis

Infrared spectroscopic analysis was performed to determine if the gray epoxy AC coating had developed an amine exudate prior to application of the red AF coating that contributed to the poor adhesion characteristics. Because the surface of the gray epoxy was contaminated with trace residuals of the red AF containing a polyamide component, the presence or absence of amine blush could not be conclusively determined.

Conclusions

There were numerous areas around the perimeter of the ship, particularly on the port side but also on the starboard side and stern, where spontaneous disbonding and relatively poor adhesion of the black AF coating was occurring. This disbonding affected the greatest

surface area and was the coating problem/failure of greatest concern.

During sampling, it was ascertained that adhesion of the AF coating system to the underlying AC coating system was variable, ranging from spontaneous disbonding in large areas to relatively tight adhesion in other areas.

It was concluded that the poor adhesion and disbonding occurred as a result of application of the red AF first coat over the gray epoxy AC topcoat, after the gray epoxy was no longer tacky.

The adhesion variability of the AF coating observed during the course of sampling, and at least visually on portions of the ship's hull, almost certainly was a result of the variable tackiness of the underlying gray AC topcoat. Where there was a long tack time, suitable adhesion occurred. Where the AF coating was applied after the tack time had been exceeded, there was moderate to lower adhesion.

Testing also established that when there was an excess amount of Part A in the mix, the tackiness time of the gray epoxy AC coating was reduced, effectively reducing the tack window and further aggravating the adhesion problem.

SUMMARY

The spontaneous disbonding that impacted the largest area occurred where the red AF coating was applied over the gray AC coating, in the area between the deep-load line (DLL) and the water. The cause of this problem was attributed to the application of the red AF coating after the tackiness window of the gray epoxy AC coating had expired. The recoat interval study of the red AF coating applied over the gray AC coating revealed that the red AF coating had markedly better adhesion when applied two hours after application of the gray AC coating than when applied four hours and 40 minutes, six hours or eight hours after application of the gray AC coating. The tackiness/tack-free test revealed that the tackiness window of the gray AC coating was 2.5 hours. A review of the painting records revealed that the red AF coating was often applied more than 2.5 hours after the gray AC coating. Adequate adhesion would not have been achieved in these areas.

Nitrogen and infrared spectroscopic

analyses of samples of the gray AC coating and controls prepared at various mix ratios indicated that much of the gray AC coating applied to the hull had an excess amount of Part A, the pigment component that contained the polyamide and polyamidoamine resins and associated solvents. The tackiness/tack-free test established that when there was an excess amount of Part A, the tackiness time of the gray epoxy AC coating was reduced, further aggravating the adhesion problem.

A secondary coating problem was the spontaneous disbonding of the gray polysiloxane topcoat from the AC coating system in the area immediately above the DLL to approximately I-to-I-1/2 feet above the DLL. The adhesion of the gray polysiloxane topcoat to the gray AC coating was excellent in the areas above this region. Cross-sectional microscopic examination of coating chip samples revealed that one or more layers of the AF coating had been inadvertently applied to numerous areas above the DLL. When the polysiloxane was applied down to the DLL, the AF was not removed, but covered over. Disbonding occurred between the red AF layer and the gray epoxy topcoat of the underlying AC coating for the same reasons as described earlier for the spontaneous disbonding and poor adhesion of the AF coating to the underlying AC coating below the DLL.

ABOUT THE AUTHOR



Cheryl Roberts is a senior chemist with KTA-Tator, Inc. She holds Bachelor of Science and Master of Science degrees in chemical engineering and a Master of Science degree in colloids, polymers and surfaces. Roberts is an active member of ASTM International and is the secretary of the Pittsburgh Society for Coatings Technology.

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TIME AND TEMPERATURE: DON'T FORGET ABOUT HUMIDITY

BY TROY FRAEBEL, ABKAELIN, LLC

Most conversations about cure times naturally default to standard laboratory conditions of 77 F and 50-percent relative humidity (RH). However, this is seldom the case in the field. Variations in recoat windows, sweat-in or induction times and pot life due to material storage and mixing temperatures are often forgotten. Combine high humidity with low temperatures or low humidity with moisture-cured products and disasters can happen. Ever-changing weather conditions are the reason it's critical that the applicable product data sheet(s) be on the jobsite and a competent sales representative and/or technical service person be readily available.

FINAL CURE

While some coatings cure by simple evaporation of a solvent, most involve a chemical reaction. Cure is defined as the coating changing from a liquid state into a dry, stable, solid protective film¹. Both evaporation and chemical reactions are affected by temperature. As temperature increases, the speed of evaporation and chemical reactions also increases. Conversely, as the temperature decreases, the evaporation rate slows and virtually stops as is the case when water freezes. Chemical reactions require a minimum temperature to initiate and as the temperature drops, these reactions will slow and eventually stop.

Industrial coating data pages, especially

OFFICE TO FIELD: LOST IN TRANSLATION

those for plural-component materials, will often list multiple temperature ranges. For example, the data page for a standard solvent-based epoxy tank lining lists a seven-day minimum cure at 77 F/50-percent RH before immersion. Reduce the temperature to 40 F and the listed cure time is now 14 days. Heating the tank to 100 F can reduce the cure time to four days. There are solvent-based epoxies that will cure down to 0 F, but beware of the cure time. While the listed time is still seven days at 77 F, it can take as long as 30 days at 0 F. Consulting the data page and testing for cure is critical. Especially in the case of potable water, the author strongly suggests testing in accordance with ASTM D5402, "Standard Practice for Assessing the Solvent Resistance of Organic Coatings Using Solvent Rubs," in addition to observing the published cure time.

RECOAT WINDOW

For multi-coat systems, one must consider the recoat window (a period beginning at a point when a coat of paint has dried or cured sufficiently to be topcoated and ending when the coating has reached a degree of cure that topcoating is not recommended without an additional surface preparation procedure¹) before thinking about final cure. Two-component epoxy primers and intermediate coats have been and are still industrial workhorses, but care must be taken when topcoating, especially with a polyurethane. On a typical epoxy data sheet, the minimum recoat time is listed from seven to 32 hours depending on the temperature with the higher temperature, 90 F, requiring the shortest time and 50 F requiring the longest time (slowest cure). However, regarding the maximum recoat time before scarfing or using a tie-coat is required, only one interval (60 days) may be listed. If the maximum recoat time was tested in a laboratory at 77 F, how long could a painter wait before applying a polyurethane topcoat to the roof of an elevated water tank in Texas in the summer? Logically, it could be less than 60 days, as the speed of the chemical reaction would increase as steel temperatures reach well over 120 F in direct sunlight. The data sheet does, however, suggest that the painter contact the manufacturer's representative for specific recommendations.

Humidity also comes into play when topcoating ethyl silicate inorganic zinc-rich primers (IOZ). If one looks at the overcoat time intervals on a typical data sheet, they range from 1.5 hours at 104 F to 18 hours at 41 F, but IOZs require moisture to cure. When paint shops are heated in the winter, the relative humidity typically drops below the laboratory testing condition of 50-percent RH, thus slowing the cure. Paint shops often mist IOZs or wet the floors in the shop to help with the cure, but testing for cure is always a good idea before applying an epoxy or polyurethane intermediate or topcoat in the shop. The data sheet previously cited instructs the painter to test for cure according to ASTM D4752, "Standard Practice for Measuring MEK Resistance of Ethyl Silicate (Inorganic) Zinc-Rich Primers by Solvent Rub." Epoxy coatings do a very good job of preventing or slowing moisture from reaching the IOZ, which typically causes the uncured IOZ to split cohesively once stressed (e.g., strapped for loading or exposed to temperature changes). Shop-applied IOZs topcoated in the field typically see sufficient moisture to cure, so splitting is usually not encountered there.

As their name implies, moisture-cured urethanes (MCU) also require moisture to cure. As with IOZs, topcoating MCU primers with epoxy or other materials prior to cure can be disastrous because the lack of moisture essentially stops the curing process.

Painters must even be cautious with simple one-component waterborne commercial acrylic materials. Painting indoors with the HVAC system running typically yields close to laboratory conditions, so the one-hour-to-touch and four-hours-to-recoat times listed on the label can be trusted. Moving outdoors when the temperature is just above the 50 F minimum might delay the recoat until the next day. Commercial labels and data pages typically only list one temperature and humidity range, so contacting the manufacturer may be necessary when temperatures are above or below those listed.

POT LIFE

Epoxy, polyurethane, polysiloxane and other two-component materials have a limited pot life, the length of time after combining two or

more components of a multiple-component coating system that the mixed coating can be successfully applied¹. Since the mixed coating is reacting chemically, the length of the pot life is limited by the temperature. Reviewing the data sheet for a typical polysiloxane, one finds the pot life ranging from 6.5 hours at 50 F to only 1.5 hours at 86 F. Pot life is much more dependent on the temperature of the material than the temperature of the ambient air, so cooling the mixed material in an ice bath or chiller can help extend the pot life. Care must be taken to keep the material above the required reaction temperature.

INDUCTION TIME

Many two-component epoxies require time for the chemical reaction to begin prior to application. This is called the induction or sweat-in time. Again, this chemical reaction is accelerated at higher temperatures and retarded at lower temperatures, so looking at a data sheet for a low-temperature-cure epoxy, one finds sweat-in times ranging from only five minutes at 120 F to one hour at 0 F. What is not clear until one reads further, is that the material should be at least 40 F for optimal performance. Even for low-temperature-cure epoxies, it is best to store and mix them at higher temperatures to aid in initiating the chemical reaction. Epoxy chemical reactions are exothermic (they produce heat), so the recommended practice is to measure the material temperature when the material is mixed and before its use. If the temperature has increased, that is a good indication that the chemical reaction has begun and the material can be successfully applied.

HUMIDITY AND TEMPERATURE

Most data pages restrict coating application to when the RH is 85 percent or below, and the air and surface temperature is at least 5 F above the dew point. Specifications often require that these conditions be maintained through final cure, but this requirement is unrealistic, for example, when final cure for a typical outdoor polyurethane can require 10 days at laboratory conditions. Consultation with the coating manufacturer is required to obtain more realistic limitations. That being said, aliphatic polyurethane topcoats applied for aesthetic purposes

OFFICE TO FIELD: LOST IN TRANSLATION

can dull severely when exposed to early moisture. A by-product of the polyurethane reaction is the production of CO₂ gas. Moisture increases this reaction and tiny CO₂ bubbles, while not significantly detrimental to the film, are trapped in the film, reducing the sheen.

Amine-cured epoxies are subject to amine blush when exposed to condensing humidity. This is caused by the reaction of amine co-reactant with carbon dioxide and water¹. The blush, an amine carbamate, may or may not be visible, but can usually be felt as a film on the surface. If topcoated, this film can adversely affect the adhesion of the next coat. The coating manufacturer should be consulted for removal methods. If untopcoated, amine blush is typically not an issue.

CONCLUSION

It is critical to monitor ambient conditions (air temperature, relative humidity and dew point), surface temperature and material temperature during coating mixing, application and cure, especially when subsequent coats of paint are going to be applied. Relatively thin coatings quickly acquire the temperature of the surface to which they are applied regardless of the ambient air temperature or bulk material temperature. Recording surface temperature gauges are helpful in monitoring the progress toward full cure or recoat window minimums or maximums; however, when in doubt, test for cure per the ASTM or other applicable standards. Data sheets contain good information on time, temperature and humidity requirements, but only the coating manufacturer can fill in the gaps. Do not hesitate to call.

ABOUT THE AUTHOR



Troy Fraebel is the vice president of Protective Coating Services for ABKaelin, LLC. He has 30 years of experience in the protective coatings industry including extensive experience in the water, wastewater, bridge, petrochemical, power, mining and metals, and marine markets. Fraebel is an SSPC Protective Coatings Specialist, a

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task force. He has authored, co-authored, presented and published multiple industry papers and holds a B.A. from Western Kentucky University and a Master's degree in education from William Paterson College.

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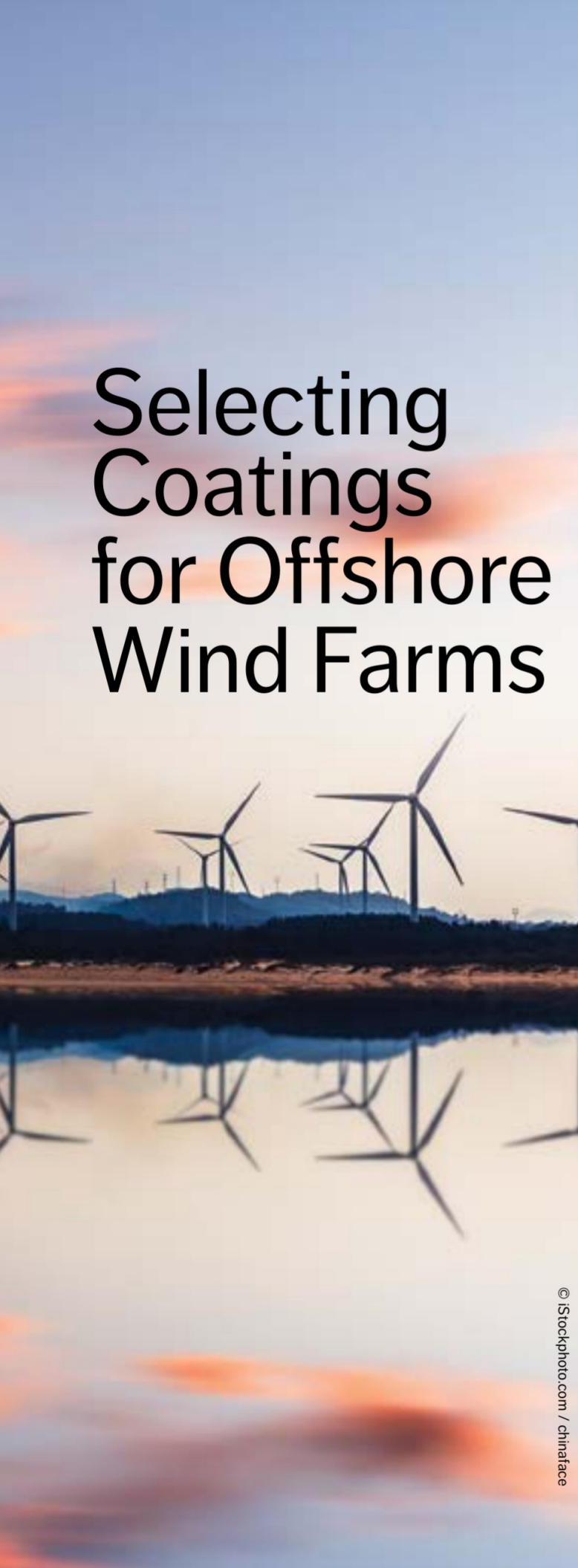
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Selecting Coatings for Offshore Wind Farms

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BY ANDERS VOLDGAARD CLAUSEN, HEMPEL A/S

In 2017, 4,331 megawatts (MW) of wind power was installed globally — a 95-percent increase over the prior year, with 84 percent (15,780 MW) of all offshore facilities located off the coasts of 11 European countries and 16 percent mostly off the coast of China with the remainder in other Asian countries¹.

According to the U.S. Office of Energy Efficiency and Renewable Energy, the U.S. has 28 projects in progress and development totaling 23,735 MW of power. Those in the near term are primarily concentrated in the North Atlantic with others in various stages of evolution in the Great

Lakes, the West Coast and Hawaii².

In Europe, 17 new wind farms were constructed in 2017, including 560 new offshore wind turbines, producing a record 3,150 MW of additional capacity. This positive growth in the European offshore sector has been driven by falling costs alongside advancements and innovation in cost-out measures (calculating total cost in advance) achieved through a greater understanding of the key risks in offshore wind tower construction, with larger projects leading to greater economies of scale and an oversupply in the wind turbine market. Offshore wind energy is projected to become Europe's fastest growing renewable source.

The rise in offshore wind energy has spurred a similar growth in related protective coatings. Although the offshore wind industry is known to be generally conservative, its search for cost savings has encouraged coatings manufacturers to research and develop new and innovative materials that can be applied more quickly, and that offer optimal protection.

ABOVE- AND BELOW-WATERLINE COATINGS

Offshore wind farms undoubtedly face some of the most severe operational and environmental conditions on the planet, constantly exposed to a corrosive marine atmosphere. Due to their locations, these structures are often difficult to access and therefore, maintenance and recoating a structure in-situ can be extremely challenging and costly, making coating selection of the utmost importance.

Experience shows that to achieve maximum protection, wind farm tower foundations have been coated with a heavy-duty epoxy paint system, and the tower structure itself with a zinc-epoxy three-coat system.

An inspection was recently carried out at the Tunø Knob offshore wind farm in Denmark, one of the world's longest-serving installations. Four of the 10 turbines were chosen at random and evaluated via visual examination, photographic documentation and dry-film thickness (DFT) measurement. Despite being more than 20 years old, the inspection found that both the interior and exterior coating systems were in good condition and could be expected to remain so for at least another 10 years, demonstrating a practical coating lifetime of more than 30 years. In the same year, the Horns Rev 1 wind farm, located in the Danish waters of the North Sea, was also inspected. In this hostile region, the environment has been classified under the ISO 12944-Part 2 standard, "Paints and varnishes

μm (2.4-to-3 mils) DFT, a two-component polyamide adduct-cured, high-solids, high-build epoxy intermediate at 140-to-180 μm (5.5-to-7.1 mils) DFT, followed by a two-component acrylic polyurethane top-coat, cured with aliphatic isocyanate at 60-to-80 μm DFT. This system method has been tried and trusted for many decades.

Although traditional zinc coatings have worked well, operators are always looking for systems that provide easier application without sacrificing corrosion protection. This article describes an innovative technology that has been developed to deliver improved corrosion resistance throughout the total lifetime of a turbine tower and meet the operator's precise requirements.

INNOVATIVE TECHNOLOGY

Zinc-rich primers have been used for many years and have proven to be an established method of corrosion protection for steel.

These systems use high levels of zinc dust as a pigment in an organic binder (epoxy) or inorganic binder (silicates) to create a galvanic effect that protects the underlying steel substrate from corrosion. The zinc particles are more active than steel and act as anodes in the coating and corrode in place of the steel when exposed to water, oxygen and/or chlorides.



Fig. 1: Coating comparison after salt-spray testing. Figures courtesy of the author unless otherwise noted.

— Corrosion protection of steel structures by protective paint systems — Part 2: Classification of environments" as C5M — a very highly corrosive marine environment with high salinity. Once again, four wind turbines were chosen at random and evaluated. The exterior and interior coated surfaces again were found to be in prime condition and from the overall results, it was estimated that the coating system would have a service life of at least 27 years in this environment.

Typical three-coat systems that deliver protection in this tough offshore environment include a zinc-rich epoxy primer at 60-to-80

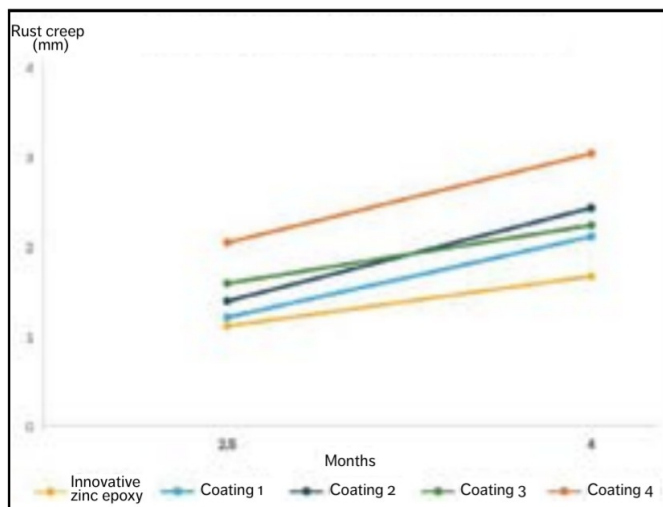


Fig. 2: Coating comparison after cyclic corrosion testing.

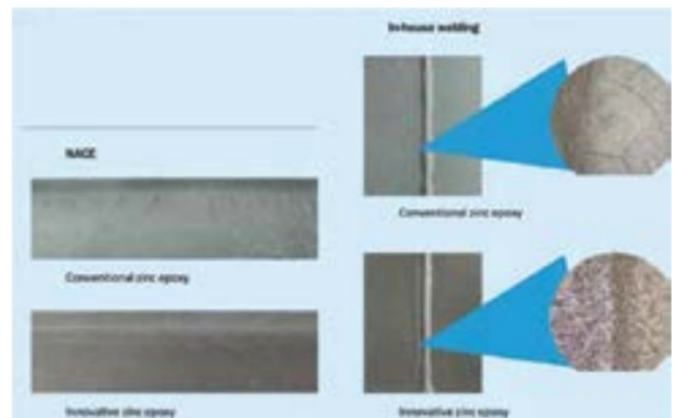


Fig. 3: Results of the NACE cracking test (TMO304-2004, "Offshore Platform Atmospheric and Splash Zone Maintenance Coating System Evaluation") and an in-house welding test.

Organic zinc-rich primers are often preferred over inorganic zinc-rich primers because they are less sensitive to surface preparation, over-application and humidity, making application easier. In 2007, research began to examine ways to improve the effectiveness of conventional zinc-rich epoxy coatings, and an important discovery was made. While a conventional organic zinc-rich epoxy coating contains approximately 80-weight-percent zinc, just one-third of that zinc actually contributes to corrosion protection. The research showed that only the zinc located in the 20-to-30 μm (0.8-to-1.2 mils) closest to the steel was consumed by the galvanic reaction in a zinc-rich coating with a DFT of 60-to-80 μm . Therefore, about 60 percent of the

zinc added to the primer was not used in the galvanic reaction.

This led to the development of an activated zinc-rich epoxy primer coating technology that incorporated tiny hollow glass spheres (approximately 40 µm [1.6 mils] in size) and a proprietary additive or "activator." Because of the synergy of these components, this coating is said to deliver three methods of corrosion protection: a galvanic effect, a barrier effect and an inhibitor effect.

For galvanic protection, the activator increases the zinc's ability to carry the corrosion current throughout the coating even if the zinc particles are not in direct contact with each other, improving the cathodic protection (CP) of the steel. The corrosion product of the zinc delivers the coating's barrier properties and self-healing characteristics. Typically, the corrosion product of a zinc-rich primer is zinc oxide. The corrosion product in this activated zinc-rich primer, however, created a more insoluble salt, zinc-chloride-hydroxide hydrate. This insoluble salt forms a uniform protective layer on the surface of the primer that acts as a barrier blocking water, oxygen and chlorides from reaching the steel surface. Additionally, by-products from the rapidly corroding activated zinc fill any cracks caused by mechanical damage in the coating, essentially enabling the coating to heal itself.

The hollow glass spheres improve the film's crack resistance by blocking the propagation of micro-cracks and contribute to the coating's low permeability.

Additionally, the glass spheres enhance the coating's inhibitor effect. An accumulation of insoluble complexes of zinc, oxygen and chlorides on the surface of the glass spheres becomes part of the coating instead of reaching the steel substrate. The zinc corrosion product created during galvanic corrosion also acts as an environmental scavenger by capturing chloride ions as they diffuse into the coating from the environment. This is the inhibitor effect, the third type of protection offered by the innovative coating.

Figure 1 compares this coating to conventional zinc epoxy after salt-spray testing (ISO 12944-6, "Paints and varnishes — Corrosion

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protection of steel structures by protective paint systems — Part 6: Laboratory performance test methods”), as well as reduced rust creep and better protection in cyclic corrosion testing (ISO 20340, “Paints and varnishes — Performance requirements for protective paint systems for offshore and related structures,” which was replaced in 2018 by ISO 12944-9, “Paints and varnishes — Corrosion protection of steel structures by protective paint systems — Part 9: Protective paint systems and laboratory performance test methods for offshore and related structures”) and NORSOK Standard M-501 Edition 6 (2012), “Surface preparation and protective coating) (Fig. 2, p. 18).

This innovative epoxy technology has been designed to release the internal stresses of continual expansion and contraction of the metal surface and the coating. This low cracking tendency can be seen from the results of the NACE cracking test (TM0304-2004, “Offshore Platform Atmospheric and

Splash Zone Maintenance Coating System Evaluation”) and an in-house welding test at various film thicknesses (Fig. 3, p. 18).

BEYOND SCIENCE: EFFICIENCY GAINS

With the need for superior protection, wind farm operators are increasingly demanding more efficient coating systems that are easy to apply and save time and money. This zinc-rich-based coating can be applied at high temperatures and humidity levels without blistering, has a recoat interval of one hour at 68 F (20 C) and dries 50 percent faster than most zinc-rich epoxy primers at similar temperatures. Its high DFT also means that it is less susceptible to cracking.

CONCLUSION

Offshore wind farms require high-performance coatings that can protect the structures for their entire service lives with minimal or no maintenance. New and innovative

paint technologies are being developed that deliver this requirement, enabling facility owners to reliably protect their assets.

ABOUT THE AUTHOR



Anders Voldsgaard Clausen has over 10 years of experience in the wind industry, working with wind companies such as Siemens, MT Højgaard and, most recently, Hempel A/S.

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Wastewater Clarifiers: Understanding Corrosion Mechanisms

BY D. A. SHERMAN, P.E. AND R. A. NIXON,
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Clarifier mechanisms have historically been fabricated from steel, utilizing a protective coating system in an attempt to prevent corrosion. Technological advances have resulted in coatings that last longer and require less maintenance. Over the years, hot-dip galvanized (HDG) coatings have competed with more traditional organic coatings. Even more current is the move to stainless steels, including austenitic (e.g., 304, 316) and duplex (e.g., 2205) alloys.

Each of these materials has advantages and disadvantages when it comes to performance, maintainability and life-cycle cost. Navigating these differences, along with comprehending the variability in clarifier environments, can make material selection quite complicated. Studying the corrosion mechanisms and root causes of numerous failed or severely corroded clarifier mechanisms has revealed several guidelines that should be understood and utilized by design engineers involved in new or rehabilitation design.

The first step is comprehension of material/environment interactions and how changes in either of them — sometimes even subtle changes — can have major consequences.

GENERAL CLARIFIER ENVIRONMENT

Corrosion of carbon steel immersed in wastewater clarifiers is mainly oxygen-driven, so corrosion rates are largely determined by how much oxygen (O_2) gets to the surface of the metal. In general, aerated wastewater is only mildly oxidizing and, with wastewater temperatures rarely exceeding 100 F (38 C), oxygen-driven corrosion of bare steel is fairly slow, generally less than 0.01 inch per year (10 mils per year). Some treatment plant processes generate higher dissolved O_2 levels in the wastewater, such as pure oxygen treatment¹. In these cases, carbon steel corrosion rates can be higher. Stainless steels generally do not corrode in such aerated, aqueous conditions at near-neutral pH, unless other conditions promote problems.

Where aeration is not assured, especially under deposits and in stagnant conditions, acidic environments can develop, often containing sulfide and other aggressive ions. In such conditions, microbiological reactions can create microenvironments corrosive to carbon steel and sometimes also to stainless steel. From a corrosion perspective, the most important types of bacteria in wastewater are those that metabolize sulfur compounds to produce acidic conditions that are corrosive to carbon steel and stainless steel. Some other bacteria oxidize ferrous ions to ferric ions, which makes the local environment more corrosive to carbon steel as well.

Differential aeration effects influence corrosion in wastewater treatment clarifiers. Aggressive cells can be established between the rake arm surfaces within the sludge layer and those rake arm surfaces above the sludge. The surfaces in the sludge corrode faster than the surfaces above the sludge because of differential aeration and/or concentration effects. These effects increase the open circuit potential difference between the two regions, one cathodic (passive) and the other anodic (active). "Potential" is the term used to describe the electromotive voltage of the metal at anodic or cathodic sites.

The pH of domestic wastewater normally is 6 to 8, running slightly on the alkaline side of neutral where there is higher use of

soaps and household cleansing materials.

Corrosion rates for steel tend to increase with decreasing pH. Dissolved carbon dioxide (CO_2) concentrations in wastewater can depress pH, especially where covered tanks do not allow the CO_2 to dissipate into the air, but rather remain dissolved as carbonic acid. This is common in pure oxygen reactors upstream of secondary clarifiers. A great deal of CO_2 also evolves from the bacterial metabolism of organic compounds during secondary biological treatment. Experience shows that dissolved CO_2 concentration has a greater impact on the corrosion of zinc than bare carbon steel.

The electrolyte is very conductive in both the primary and secondary stages of treatment. This conductivity increases with high dissolved chloride, sulfate and sulfide concentrations. Accordingly, wastewater treatment plants served by collection systems with greater coastal infiltration can suffer higher metal corrosion rates. Also, treatment plants that use more ferric chloride for promoting flocculation in the clarifiers, or for reducing dissolved hydrogen sulfide (H_2S) concentrations upstream of the clarifiers, will tend to have higher carbon steel and stainless steel corrosion rates.



Fig. 1: Pitting at breaches in the coating typically has relatively high corrosion rates due to the large cathodic (coated steel) area relative to the very small anodic (coating failure or lack of coating) area as shown. All figures courtesy of the author unless otherwise noted.

Corrosion rates for submerged steel tend to be greater at higher elevations in the wastewater, where dissolved O_2 contents are greater. Corrosion rates also increase with radial distance from the center of the



Fig. 2: This photo shows below-waterline corrosion at areas of coating failure.

clarifier, as the relative velocity between the rake arm and water increases. For example, an increase in velocity from 0 to 0.25 feet per second — which can occur between the center column and the tip of the rake mechanism — can double the corrosion rate of bare steel. Increasing velocities affect the ability of protective scales to form and remain adhered to the steel surface.

The major difference in corrosion mechanisms between primary and secondary clarifiers involves biogenic sulfide corrosion. This is a gas-phase or vapor-phase corrosion problem whereby sulfuric acid is formed through the biogenesis of H_2S by sulfur-oxidizing bacteria. This occurs in the aerated headspaces of covered primary clarifiers. Biogenic sulfide corrosion causes rapid corrosion rates of bare carbon steel in these clarifier headspaces.

By the time the wastewater reaches aeration or pure oxygen exposure in the secondary stage of treatment, the reducible H_2S and other sulfur species are largely gone or have been reduced substantially upstream of the secondary clarifiers. In secondary clarifiers, the corrosion mechanisms above the waterline generally are oxygen-driven and influenced by weathering exposure and high humidity from the evaporative vapors from the wastewater.

MATERIALS AND THEIR SPECIFIC ISSUES

Most of the information presented previously is with regard to the corrosion of bare carbon steel, which is not typically found in clarifiers,



Fig. 3: Attention to detail is required to assure good film quality.

except where protective coatings have failed. Discussed later are organic and HDG coatings, along with solid stainless steel as alternatives to uncoated carbon steel.

Coated Carbon Steel

As discussed previously, the immersed components of coated steel mechanisms are prone to oxygen-driven electrolytic corrosion. Coated carbon steel below the waterline is also susceptible to under-deposit pitting corrosion in both primary and secondary clarifiers. This corrosion involves differential oxygen concentration cells and can be microbiological in nature, as well. Both mechanisms result in pitting corrosion, which occurs at breaches in the coating. This pitting typically has relatively high corrosion rates due to the large cathodic (coated steel) area relative to the very small anodic (coating failure or lack of coating) area as shown in Figure 1.

The organic resin-based coatings most widely used today on steel in clarifiers are based on epoxy and polyurethane chemistries. The epoxy-based coatings have mostly replaced coal-tar epoxy formulations, once the mainstay for clarifier steel corrosion protection. These newer epoxy coatings have good water resistance, excellent chemical resistance and good film-build properties (12-to-30 mils per coat). The epoxy products are mainly used below the waterline, while epoxy first coats followed by an acrylic aliphatic polyurethane finish coat are chosen for areas above the waterline. The polyurethane provides UV light resistance and good

color/gloss retention where epoxies tend to chalk when exposed to sunlight. Some coating systems also utilize moisture-cured polyurethane primers followed by epoxy or polyurethane coats.

The main performance objective for coatings is to provide barrier protection and isolate the steel from the wastewater or headspace environment. To achieve this, the coating film quality must be ensured. This means minimizing pinholes or discontinuities in the film. This is difficult in clarifier construction because of the steel shapes used to fabricate rake arms and other clarifier mechanism components. Figure 2 demonstrates below-waterline corrosion at areas of coating failure. Angles, channels and other flanged shapes provide numerous edges, corners, nooks and crannies. Therefore, to achieve good film quality on these structures, great care must be taken in selecting and applying these coatings. Figure 3 demonstrates the attention to detail required for assuring good film quality. Coatings that provide better edge retention and film build per coat are the best choices. Stripe coating of the edges and corners is highly recommended to assure that good film quality and necessary film thickness are achieved (Fig. 4). Preventing pinholes, discontinuities and misses in the coating system is crucial for good barrier protection. This focus on film quality and proper surface preparation are the hallmarks of good coating system performance in clarifiers.

Most properly selected and installed



Fig. 4: Stripe coating the edges and corners is highly recommended to assure that good film quality and necessary film thickness are achieved.

organic coating systems perform well in clarifiers for about 15-to-18 years before major coating repair work or recoating is required. Ongoing coating system inspection and more frequent coating system repairs have been shown to extend system performance at a lower overall life-cycle cost for up to 25 years.

Protective coatings do not tend to fail from chemical degradation over time in clarifier service. Rather, coatings tend to age-harden, embrittle or disbond due to undercutting corrosion that initiated at pinholes in the coating film.

Hot-Dip Galvanizing (HDG)

HDG represents the other most common corrosion barrier for carbon steel in general. HDG steel is a process whereby the steel is acid-pickled (to prepare the surface) and dipped in molten zinc to form a zinc and iron alloy that has very good adhesion to the steel surface. When cooled, there is not a clear line of demarcation between the zinc and the steel, but rather a gradual transition of the zinc and iron alloy (Fig. 5, p. 26). Starting at the bottom is the steel substrate. Next is a thin layer (gamma) that is typically 25-percent iron and 75-percent zinc, followed by the delta layer that is 90-percent zinc and 10-percent iron. Then comes the zeta layer that is about 94-percent zinc and 6-percent iron, with the final, eta layer at the top being 100-percent zinc. This is important to know because corrosion of the zinc and iron alloy can look like corrosion of the carbon steel

base metal, especially at the lower layers (gamma and delta).

Zinc coatings are protective in two very different ways. First, they serve as a barrier coating to prevent the steel from contact with the electrolyte. Secondly, they act as a galvanic protector of the steel because they corrode preferentially to the steel when both metals are active in a common electrolyte and electrically coupled.

Zinc's corrosion resistance is owed to the formation of an

insoluble basic carbonate film in the case of atmospheric exposure. The contributing factors that affect the formation of that film follow.

- Duration and frequency of moisture contact (time of wetness).
- Rate of surface drying.
- Extent of exposure to corrodents.

In atmospheric exposures (that are not corrosive), zinc reacts with air to form zinc oxide (ZnO) and later zinc hydroxide (Zn(OH)₂). Ultimately, it reacts with atmospheric CO₂ to form zinc carbonate (the most protective film). If moisture is present, increasing times of wetness correlate to increasing corrosion. If the atmosphere is not especially aggressive, the zinc forms a white powdery corrosion product called white rust. It is voluminous and does not permit the formation of a tightly adhered oxide film. This is not necessarily a major corrosion concern, but it does prevent the formation of a good barrier and keeps moisture present. This means more time of wetness and, over time, more corrosion.

For submerged conditions, the corrosion of zinc in water is mostly related to the impurities in the water, although pH, time of exposure, temperature and motion (or agitation) are other contributing factors. As in atmospheric exposure, the corrosion resistance of zinc in waters largely depends on its initial ability to form a protective layer or film, such as calcium carbonate (CaCO₃). In the case of distilled water, for example, there is no chance of the formation of a protective scale. Hence, the access of O₂ to the zinc surface is unimpeded and corrosion is quite severe. The scale-forming capability of water depends for the most part on the three following factors.

- Hydrogen ion concentration (pH).
- Total calcium content.
- Total alkalinity.

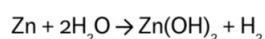
If the pH of the water is below where the water can be in equilibrium with CaCO₃, the water will dissolve the scale rather than deposit the scale. And while hardness and alkalinity are very important, and harder waters are better than softer waters, other factors must be considered. For instance, it is known

Table 1: Effect of Oxygen on the Corrosion of Zinc in Distilled Water.

Test Condition	Temperature	Corrosion Rate, Micrometers/Year
Boiled distilled water – specimens in sealed flasks	72 F	25.4 (1 mpy)*
Oxygen slowly bubbled through distilled water	72 F	218.4 (8.6 mpy)*

*mpy = mils (0.001 inch) per year

empirically that waters high in free CO₂ are aggressive toward zinc. Also, waters higher in dissolved O₂ are more aggressive to zinc than those with lower dissolved O₂. The corrosion of zinc in water follows this reaction.



This reaction is complicated when lots of O₂ is present. The O₂ depolarizes and accelerates the corrosion reaction by combining with the evolved hydrogen. The end result is that the corrosion is largely driven by how much oxygen gets to the metal surface, which is the same driver of corrosion of uncoated steel in most waters. As reported in *Uhlig's Corrosion Handbook*², the effect of oxygen on the corrosion of zinc in distilled water is demonstrated in Table 1.

Normal tap water at room temperature has a dissolved oxygen concentration of approximately 4-to-8 mg/L, which results in a theoretical corrosion rate for zinc of up to 3-to-4 mils per year. The zinc in the most aerated regions of clarifiers (typically near the inlet at the center well) would experience the highest corrosion rates where the dissolved oxygen concentration would likely be 8 or 10 mg/L.

As mentioned previously, the pH of the water is critical to zinc corrosion and scale formation. It has generally been shown that zinc performs well at a pH of between 6 and 12, assuming no other corrosion contributors are present. But, that is not the case in wastewater clarifiers.

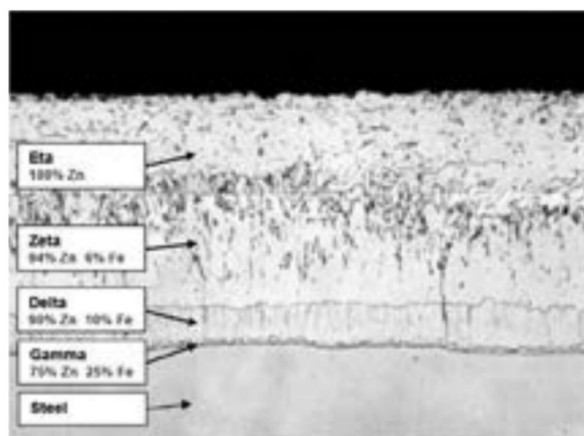


Fig. 5: HDG steel is a process whereby the steel is acid-pickled (to prepare the surface) and dipped in molten zinc to form a zinc and iron alloy that has very good adhesion to the steel surface. When cooled, there is not a clear line of demarcation between the zinc and the steel, but rather a gradual transition of the zinc and iron alloy.

HDG typically produces an approximate upper coating thickness range of 4-to-6 mils. ASTM A123 requires about 3-to-4 mils of total zinc coating thickness for steel components³. However, only the outer 1.5 mils or so of that represents pure zinc. Below that, the layers of the HDG come with increasing concentrations of iron and, once the iron-zinc layers of the HDG coating become exposed, the factors that influence carbon steel corrosion come into play as well.

An understanding of the combined influence of pH, calcium hardness, alkalinity, total dissolved solids concentration and temperature is essential in discerning the corrosiveness of any water towards zinc. Those parameters can be utilized to examine the CaCO₃ stability of the wastewater in accordance with the Langelier, Ryznar, and Practical Saturation Indices (calculations for the propensity for water to precipitate calcium carbonate onto the metal surface providing a protective barrier) to discern if the water would tend to form a protective CaCO₃



Fig. 6: HDG corrosion in the secondary clarifier rake mechanism. Note that the corrosion rate has varied in the various HDG layers.

scale on HDG steel. This is typically not the case in municipal wastewaters.

Another factor to consider for the corrosion of zinc includes chloride ion concentrations in the water. Where waters do not have the tendency to precipitate calcium carbonate scale, it has been reported that chloride ion concentrations of 50 mg/L or higher can be corrosive to zinc⁴.

Repair of HDG steel generally requires blasting and coating using a suitable organic coating system. The damaged HDG layer must be removed in its entirety. Coating over galvanizing is fraught with problems. Repair of small areas of failed galvanizing with field-applied galvanizing products can be done successfully with the right products and surface preparation; however, wholesale galvanizing of large structures in the field should be avoided.

Figure 6 shows the active corrosion of HDG coatings in a secondary clarifier rake mechanism and stilling well after only one year in service. Where the HDG coating thickness was appreciably greater, the corrosion had not yet progressed into the lower delta or gamma layers.

Stainless Steel

In general, stainless steels avoid the general corrosion issues that plague bare or HDG steels in wastewater clarifiers. Stainless steels are iron-based alloys containing more than 11-percent chromium; this forms a thin, protective oxide film, which is the reason why this group of steels has their characteristic stainless nature or corrosion resistance.

The ability of the oxide layer to heal itself (in most exposures) means that the steel is corrosion-resistant no matter how much of the surface is removed. This is not the case when carbon steel is protected from corrosion by HDG or organic coatings.

The passive oxide film on stainless steels prevents corrosion except where certain exposure conditions cause it to break down or

where it cannot be restored naturally. The most notable examples of these conditions include exposure to certain concentrations of chloride ions and microbiologically influenced corrosion. In addition, the presence of crevices or rough edges exacerbates corrosion under these conditions⁵.

Chromium, nitrogen and molybdenum contents in the alloy are largely what

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differentiate types of stainless steel with respect to pitting and crevice corrosion resistance. The major compositional difference between Type 304 and Type 316 stainless steels is the molybdenum content: 304 contains no molybdenum whereas 316 contains 2-to-3 percent. This makes the localized chloride-related corrosion (pitting, crevice) resistance of 316 superior to that of 304, as demonstrated in Figure 7.

While pH and temperature affect stainless steel corrosion, chloride concentration is the factor that most significantly promotes the breakdown of passivity and enhances the corrosion rate in clarifiers. Pitting and crevice corrosion occur when the passive oxide film is disrupted or broken down by chloride ions or other chemical species aggressive to the passivity. Certain chloride ion concentrations have been shown to initiate pitting and crevice corrosion in various stainless steel alloys under specific pH and temperature conditions. Extensive metallurgical and electrochemical testing has demonstrated that there are critical pitting temperatures, critical crevice corrosion temperatures and corrosion threshold chloride concentrations for the different stainless steel alloys. These limits can be obtained from published data or laboratory corrosion testing. Also, corrosion engineers use a value called the pitting resistance equivalent number (PREN) to compare localized corrosion resistance for the various

Table 2: Stainless Steels: Chemistry, Chloride Pitting Resistance and Cost.

Stainless Grade Steel	UNS ¹ Number	Cr % (Typ.)	Mo % (Typ.)	PREN ²	Approx. Cl ⁻ Concentration Below Which Pitting Does Not Occur (ppm) ³	Relative Cost (304 = 1.0)
304L	S30403	18	0	18	300	1.00
316L	S31603	17	2.1	23	1,000	1.27
317LMN	S31726	18.5	4.1	32	5,000	2.28
2205	S32205	22.5	3.3	34	5,000	1.24
AL6XN	N08367	20.5	6.1	43	Seawater level concentrations	3.66

1 UNS = Unified Numbering System.

2 PREN = Pitting Resistance Equivalent Number; %Cr + 3.3·%Mo + 16·%N, based on minimum composition.

3 At 90 F.



Fig. 8: Chlorides concentrate on stainless steel surfaces, especially at the water line and where metal surfaces are hot from direct sunlight exposure.

chlorides to concentrate. This creates localized places where the chloride concentrations can exceed the metal's pitting resistance. There are no better crevice conditions than threaded fasteners or flanged-gasketed connections.

In addition, pitting corrosion tends to initiate at welds for metallurgical reasons. Weld metals and the heat-affected zones associated with those welds are less corrosion-resistant than the base metal. This has to do with metallurgical alterations created by weld heat, including segregation of the chromium at the metal surface.

Various process conditions can result in concentration effects with chlorides. These conditions can include wet/dry cyclic conditions, particularly common at or just above the water line in uncovered clarifiers in arid climates. At such locations, the chlorides concentrate on the stainless steel surfaces, especially where metal surfaces are hot from direct sunlight exposure (Fig. 8). Where this concentration occurs, chloride levels can be many times greater than in the bulk wastewater. This can lead to severe pitting corrosion. Again, this is particularly problematic at crevice locations such as flanged connections or on threaded fastener surfaces.

Microbial action can also promote the corrosion of stainless steel. This generally involves bacteria that metabolize (by reduction) sulfur compounds to produce sulfides in local environments on the metal surface. The latter condition produces oxidizing corrosion potentials. These bacterial corrosion

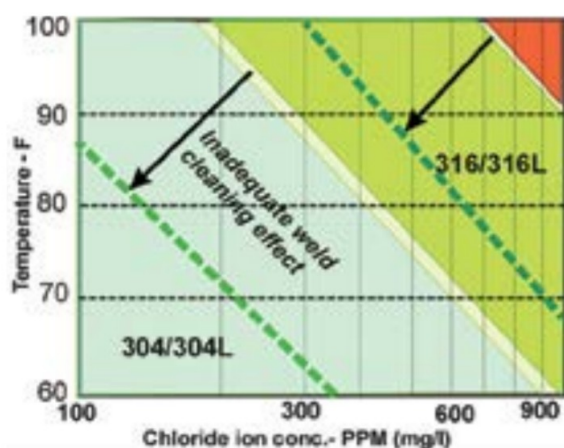


Fig. 7: This figure demonstrates general usage zones for 304/304L and 316/316L stainless steels in aerated, chloride containing natural waters with pH 5-9. Harmful effects of heat scales and surface contamination from welding on resistance to localized corrosion is mitigated to different degrees by different post-weld cleaning methods.

stainless steel alloys. This comparison is based on exposure to chloride-containing environments. Table 2 presents the PREN for the stainless steel alloys most likely to be considered for clarifiers, assuming neutral pH and a temperature of 90 F (35 C). Approximate limiting concentrations for the chloride ion and relative cost also are listed⁶.

Pitting corrosion of stainless steels typically begins where deposits attach to the metal surface or where rough areas, such as welds, exist. Roughness and crevices are ideal environments for localized pitting and crevice corrosion. The passivity of the metal surface at rough areas is breached more readily, and crevices and rough surfaces enable

processes drive microbiologically influenced corrosion (MIC). The sulfur-reducing environments produce highly acidic, under-deposit (beneath biofilm) conditions, which detrimentally affect passivity.

MIC occurs most often in primary clarifiers where stagnant or quiescent flow and anaerobic conditions are present, at mostly ambient temperatures (within the sludge blanket). The corrosion rates can be extremely high. MIC also tends to develop at rough areas or at crevices, both of which are hospitable to microbial attachment and colonization. Typical examples include rough grind marks on rolled steel or stainless steel structural members, or the threads of fasteners.

The 300-series stainless steels and 2205 duplex stainless steel are susceptible to MIC. Immunity to MIC typically requires an alloy that has a PREN of at least 40. This brings us to very expensive stainless steel alloys such as the so-called six moly stainless steels (AL6XN or 254SMO) or super-duplex stainless steels such as Type 2507.

Stainless steels such as 304 and 316 tend not to suffer from localized corrosion when fluid velocity is at least 5 feet per second. Fluid velocity in clarifiers is rarely this high except at the center inlet area.

The corrosion resistance of welds is always lower than that of the same alloy's base metal. Thus consideration should be given to upgrading the weld filler metal to enhance the corrosion resistance of stainless steel welds. For example, 316 electrodes would be used for 304L welds and 317 electrodes for 316L welds.

Maximizing the corrosion resistance of stainless steel welds also necessitates proper post-weld surface preparation and cleaning during fabrication (shop) and erection (field). This starts with careful mechanical removal of all weld slag, including grinding to remove weld spatter and rough weld areas. Additionally, all heat tint (bluish hue on the metal surfaces) should be removed by grinding and/or grit/bead blasting, followed by acid pickling to remove any remaining free iron. If not properly cleaned, these areas will be susceptible to localized corrosion due to

the reduced resistance of this chromium-depleted metal surface area.

OTHER MATERIALS CONSIDERATIONS

Galvanic Effects

Electrically connected, dissimilar metals immersed in either primary or secondary clarifiers create ideal conditions for galvanic corrosion. Galvanized steel generally does poorly in

these environments and carbon steel readily corrodes preferentially to stainless steel.

As with all galvanic corrosion, the rate is mainly governed by the electrochemical potential difference between the two electrically continuous metals, their proximity to one another and the anode-to-cathode area ratio (a small anode with a large cathode is the worst combination).

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CORROSION IN WASTEWATER CLARIFIERS

The most common galvanic corrosion observed in wastewater clarifiers is localized pitting of carbon steel (at coating breaches) near stainless steel components like suction tubes. Because suction tubes cannot be re-coated on the interior after initial construction, stainless steel has become the standard material of choice. Electrical isolation of the stainless steel suction tube from the coated carbon steel is necessary to prevent galvanic corrosion.

Sometimes, failed carbon steel structural members on rake arms are replaced with stainless steel, which will affect corrosion of connected carbon steel components.

The corrosion rate of the anodic material will generally be highest at the dissimilar metal connection and decrease with increasing distance away from the connection. Electrical isolation between dissimilar metals can be achieved at bolted connections by installing isolation bolt kits. However, the insulating spacers can degrade over time and re-introduce electrical continuity. If only welded connections exist, stainless steel in contact with coated carbon steel can be coated at the connection, plus some distance beyond the connection to achieve effective electrical isolation.

SUMMARY

When selecting materials for construction for wastewater treatment plant clarifier mechanisms, one must understand the operating environment, the candidate materials and their properties, and the damage mechanisms caused by interaction between those materials and the environment. Also important are fabrication and erection practices and their effects on corrosion resistance of the materials.

Carbon steel protected by a suitable organic coating system remains a viable option for both new and rehabilitation construction. A tight and enforceable specification for the work, along with good quality control during fabrication and erection are crucial for long service life. Still, the nature of such coatings makes periodic inspection (with the associated costs for dewatering, cleaning and access) necessary, and the best coatings will

likely last less than 20 years if not well-applied and well-maintained.

HDG steel is an alternative to coated steel, but will have a high susceptibility for failure in most wastewater clarifier environments. The fact that the coating is metallic brings into play more issues than for organic coatings, such as scale formation and galvanic effects. As with organic coatings, regular inspection is required. Additionally, when the galvanizing finally goes away, it cannot be replaced with new galvanizing. Using HDG for clarifier mechanism corrosion protection can be done if all the conditions are right, but it is very risky.

Stainless steels are a step above coated steel in most cases. The higher initial material costs are typically offset within the first 10 years of clarifier operation by lower inspection and repair costs. Stainless steels, though, can have issues — expensive ones — if not selected properly for the operating conditions and/or if not fabricated so as to eliminate those issues. Again, a tight and enforceable material and fabrication specification, along with good quality control during fabrication and erection, are crucial.

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2018

The Annual Equipment Buying Guide

The *JPCL* Equipment Buying Guide lists equipment and related supplies for protective and marine coating work from more than 350 manufacturers, distributors and rental companies, published annually to assist our readers in the identification of equipment and supplies for protective and marine coating operations.

On p. 32, you will find the Table of Contents, where generic products are listed under nine categories: Access; Application; Climate Control; Environmental Protection Equipment; Inspection; Laboratory Testing; Safety; Software; and Surface Preparation.

On p. 33, you will find the Index to the Buying Guide, where products are listed alphabetically in a single list. Individual company profiles with contact information can be accessed on p. 108.

In the Guide itself, which begins on p. 35, companies either displayed in boldface type or accompanied by boxed display ads have paid an advertising fee. Otherwise, a company's information appears free of charge.

The Guide is based on data obtained through a survey sent in April 2018 to companies known to *JPCL*. The print edition of the *JPCL* Guide includes the companies that completed the survey by the deadline for the June 2018 issue. This Guide is also available at www.paintsquare.com/bg, the online home of *JPCL*, where information is updatable throughout the year. To participate in the online edition of the Equipment Buying Guide between print editions, please contact Nichole Altieri, business administration manager, *JPCL*, at naltieri@paintsquare.com.

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T Tex Industries LP
Temco Distributors
Titan Tool
Tritech Industries, Inc.
Uni-Royal Pack Co., Ltd.
Victory Air & Equipment, Inc.
VR Coatings Pvt. Ltd.
The Warehouse Rentals and Supplies
WIWA LLC

SPRAY SYSTEMS, ELECTROSTATIC

Abrasives Inc.
Advanced Finishing Systems, Inc.
AirTech Spray Systems
Arkco (Thailand) Co., Ltd.
Bittner's Spray Equipment Co.
BlastOne International
Bolair Fluid Handling Systems
Carlisle Fluid Technologies-Binks
CESCO - Aqua Miser
Corrosion Specialties Inc.
EnDiSys
Glenn Saren & Assoc. Inc.
Graco Inc.
IDS Blast
Jadalc
Lesoon Equipment Pte. Ltd.
Marco
Masterfield Industrial Equipment
Midwest Surface Prep, LLC
The Paint Project, Inc.
SIE Industrial Ltd.
Specialty Products, Inc. (SPI)
Spin Import Export
Surface Prep Supply
T Tex Industries LP
Temco Distributors
Titan Tool
Uni-Royal Pack Co., Ltd.
VR Coatings Pvt. Ltd.
The Warehouse Rentals and Supplies

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AirTech Spray Systems
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Arkco (Thailand) Co., Ltd.
Bittner's Spray Equipment Co.
BlastOne International
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Carlisle Fluid Technologies-Binks
CESCO - Aqua Miser
Corrosion Specialties Inc.
DUX Technologies, Inc.
EnDiSys
Glenn Saren & Assoc. Inc.
Graco Inc.
IDS Blast
Jadalc
Lesoon Equipment Pte. Ltd.
Marco
Masterfield Industrial Equipment
Mattson Spray Equipment
Midwest Surface Prep, LLC
The Paint Project, Inc.

Quikspray, Inc.



SIE Industrial Ltd.
Specialty Products, Inc. (SPI)
Spin Import Export
Surface Prep Supply
T Tex Industries LP
Temco Distributors
Titan Tool
Uni-Royal Pack Co., Ltd.
Victory Air & Equipment, Inc.
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Advanced Finishing Systems, Inc.
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Arma Coatings
Bittner's Spray Equipment Co.
Blastlink USA
BlastOne International
Bolair Fluid Handling Systems



Carlisle Fluid Technologies-Binks
CESCO - Aqua Miser
Corrosion Specialties Inc.
Dispensing Technology Corporation
EnDiSys
Gaco Western
Glenn Saren & Assoc. Inc.
Graco Inc.
IDS Blast
Intech Equipment & Supply
Jadalc
Lesoon Equipment Pte. Ltd.
Marco
Masterfield Industrial Equipment
Mattson Spray Equipment
MES Rentals
Midwest Surface Prep, LLC
Oak Ridge Foam and Coating Systems
Pacific Roller Die Company, Inc.
The Paint Project, Inc.
Remote Orbital Installations, LLC
SIE Industrial Ltd.
Specialty Products, Inc. (SPI)
Spin Import Export
Surface Prep Supply
T Tex Industries LP
Temco Distributors
Titan Tool
Uni-Royal Pack Co., Ltd.

Victory Air & Equipment, Inc.
VR Coatings Pvt. Ltd.
The Warehouse Rentals and Supplies
WIWA LLC

SQUEEGEE FLOOR COATING MACHINES

Bon Tool Co.
EnDiSys
Glenn Saren & Assoc. Inc.
Magnolia Brush
Quikspray, Inc.



SIE Industrial Ltd.
Surface Prep Supply
Victory Air & Equipment, Inc.
The Warehouse Rentals and Supplies

STRAINERS

AirTech Spray Systems
American Spray Technologies
Arkco (Thailand) Co., Ltd.
Carlisle Fluid Technologies-Binks
CESCO - Aqua Miser
Cincinnati Color Company
Corrosion Specialties Inc.
Intech Equipment & Supply
Lesoon Equipment Pte. Ltd.
Marco
MES Rentals
Midwest Surface Prep, LLC
The Paint Project, Inc.
Paul N. Gardner Co., Inc.
SIE Industrial Ltd.
Surface Prep Supply
Surface Preparation-Texas, LLC
T Tex Industries LP
Trimaco, LLC
Uni-Royal Pack Co., Ltd.
Victory Air & Equipment, Inc.
The Warehouse Rentals and Supplies

SUNDRIES

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Cincinnati Color Company
Corrosion Specialties Inc.
Glenn Saren & Assoc. Inc.
Hyde Group
Lesoon Equipment Pte. Ltd.
Magnolia Brush
Marco
MES Rentals
Midwest Surface Prep, LLC
Mr. Shrinkwrap
Nour Trading House Inc.
The Paint Project, Inc.
Shur-Line
SIE Industrial Ltd.
Sunnyside Corporation/Back To Nature Products
Surface Prep Supply
Surface Preparation-Texas, LLC
T Tex Industries LP

Trimaco, LLC



Victory Air & Equipment, Inc.
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EnDiSys
Glenn Saren & Assoc. Inc.
Jadalc
Lesoon Equipment Pte. Ltd.
Marco
MES Rentals
SIE Industrial Ltd.
Surface Prep Supply
Thermion
Titan Tool
TMS Metalizing Systems, Ltd.
Uni-Royal Pack Co., Ltd.
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Bolair Fluid Handling Systems
Carlisle Fluid Technologies-Binks
Cincinnati Color Company
Corrosion Specialties Inc.
Dispensing Technology Corporation
EnDiSys
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Intech Equipment & Supply
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Jadalc
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Marco
Newstripe
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Axxiom Manufacturing
BlastOne International
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Clemco Industries Corp.
Corrosion Specialties Inc.
DeHumidification Technologies, LP



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MES Rentals
Munters Corporation
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Rapid-Prep, LLC
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How can I save costs when using a desiccant system?

Dehumidification systems on coatings projects can be expensive. The equipment, logistic and operating costs can often make the logic to use the equipment seem unreasonable. When portable generators are necessary, fuel can be the biggest cost involved. Fortunately there are many strategies that can help to reduce this pain. Dehumidification systems can be controlled by remote sensors to turn off the heaters (propane, NG, electric) or compressors based on a preset dew point differential. This could reduce energy consumption by as much as 50% depending on outside air conditions.

Additionally creating a complete climate control plan, ensuring that your equipment is sized correctly, providing enough lead time for shipping and searching for house power are other effective ways to reduce your costs of dehumidification on your projects. Finally utilizing equipment with cost saving benefits built in to their design will help reduce overall dehumidification costs as well. Surprisingly, discounts on rental rates typically have the least impact of all the costs involved.



Quite possibly, the most important cost factor is the potential cost of losing the blast if the equipment shuts off for some reason. When this occurs, you lose time and production. This is where remote monitoring can really save the day.

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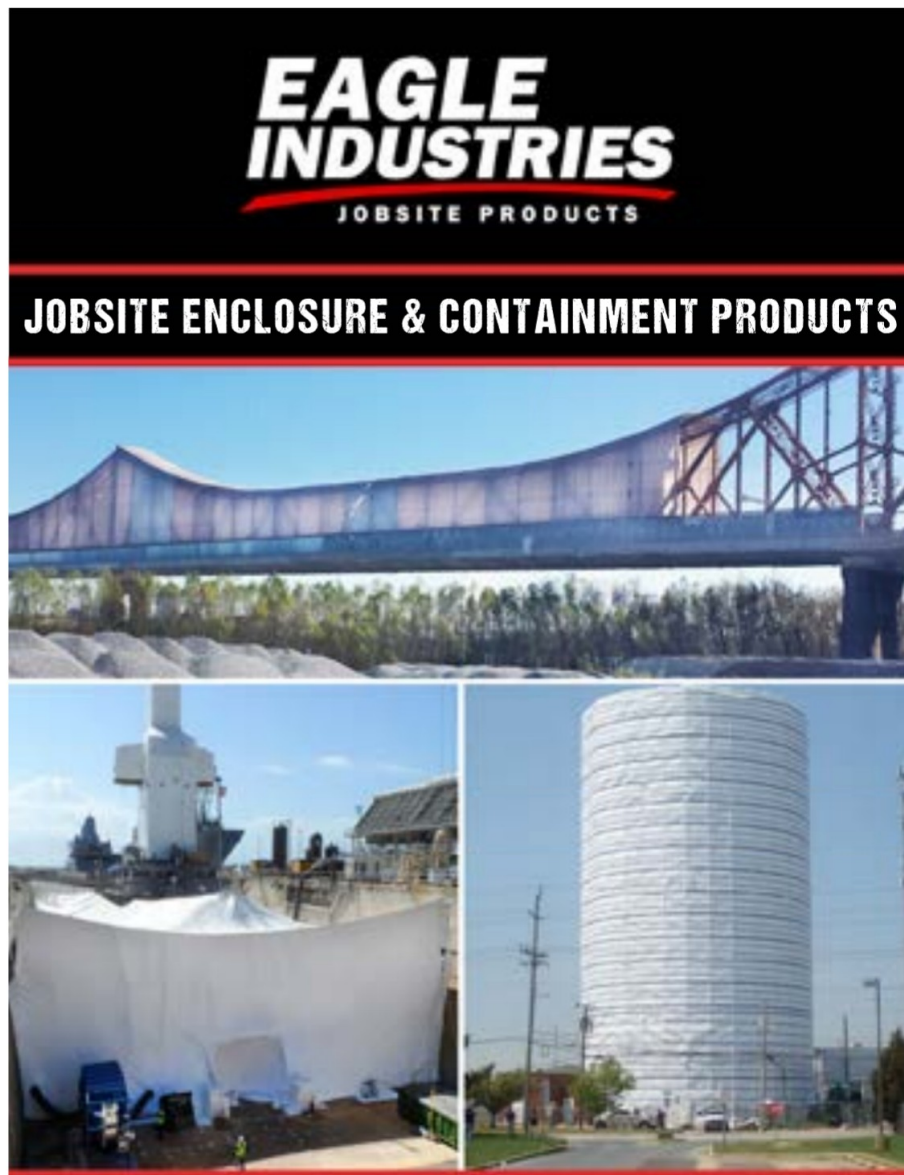
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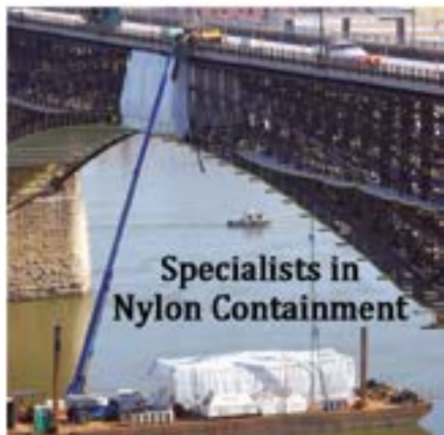
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Dry Air Technology



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Portland, OR 97217
Contact: Steve Edmondson
Phone: 503-285-0569
info@advancedfinishing.com
www.advancedfinishing.com
Rental Company

Aggreko

15600 JFK Blvd., Ste 900
Houston, TX 77032
Contact: Corporate Office
Phone: 877-244-7356
aggreko@aggreko.com
www.aggreko.com
Rental Company

Air Conditioner Rental and Leasing Inc.

1001 Freyburg Street
Pittsburgh, PA 15203
Contact: Scott Penner
Phone: 800-581-4844
sp@acrental.com
www.acrental.com
Manufacturer / Distributor / Rental Company

Air Systems International

829 Juniper Crescent
Chesapeake, VA 23320
Contact: Customer Service
Phone: 800-866-8100
sales@airsystems.com
www.airsystems.com
Manufacturer

Airblast AFC

250 Airport Parkway
Oroville, CA 95965
Contact: Jeremy Hagan
Phone: 800-331-7744
jeremy@afcfilters.com
www.airblastafc.com
Manufacturer / Distributor

Airblast B.V.

PO Box 1075
Heerhugowaard, 1700 BB
Netherlands
Contact: Mr. Nick Smith
Phone: 31-72-5718002
info@airblast.com
www.airblast.com
Manufacturer / Distributor

Airtec Ltd.

Industriestrasse 40
Zunzgen, CH-4455 Switzerland
Contact: Thomas Wyser
Phone: 41-619769525
tom.wyser@airtec.ch
Manufacturer / Distributor / Rental Company

AirTech Spray Systems

4303 Pinemont Dr.
Houston, TX 77018
Contact: Ronald CREDIT
Phone: 713-681-0013
sales@airtechspray.com
www.airtechspray.com
Manufacturer / Distributor / Rental Company

All Jetting Technologies, Inc.

2740 Martin Downs Blvd., #318
Palm City, FL 34990
Contact: Rodney Hardin
Phone: 772-286-1218
info@alljetting.com
www.alljetting.com
Manufacturer / Distributor

American Spray Technologies

1807 Pike St. NW Suite 103
Auburn, WA 98001
Contact: William Saas
Phone: 253-833-4342
info@sprayrig.com
www.sprayrig.com
Manufacturer

APE Companies

3009 Pasadena Freeway, Suite 100
Pasadena, TX 77503
Contact: Jon Randolph
Phone: 281-930-0808
jrandolph@apecompanies.com
www.APEcompanies.com
Distributor

ARID-DRY by Controlled Dehumidification

5931 Ford Court
Brighton, MI 48116
Contact: Tom Haarla
Phone: 810-229-7900
sales@ctrdrh.com
www.ctrdrh.com
Manufacturer / Distributor

Arkco (Thailand) Co., Ltd.

19/23 Moo 8 Suksawad Road SOI
84 Naiklongbangplakod Sub-
District, Prasamutjedee District
Samutprakarn, 10290 Thailand
Contact: Kevin Yeo
Phone: 66-899202257
sales@arkcothailand.com
www.arkcothailand.com
Distributor

Arma Coatings

5555 W. 11th Ave
Eugene, OR 97402
Contact: Brian Clements
Phone: 541-688-3500
sales@armacoatings.com
www.armacoatings.com
Manufacturer / Distributor

Armex

Church & Dwight Co., Inc.
469 North Harrison Street
Princeton, NJ 08543
Contact: Sales
Phone: 800-332-5424
armex@churchdwight.com
www.armex.com
Manufacturer

ARS Recycling Systems, LLC

4000 McCartney Rd.
Lowellville, OH 44436
Contact: Doug Reed
Phone: 330-536-8210
info@arsrecycling.com
www.arsrecycling.com
Manufacturer

Ascent

206 Krishnadeep Town Fatehganj
Vadodara, 390002 India
Phone: 91-11-47533108
Manufacturer

AST/Adhesive Systems Technology Corp.

1600 Freeway Boulevard
Brooklyn Center, MN 55430
Contact: Stephen Hirt
Phone: 763-592-2060
sales@ast-corp.net
www.ast-corp.net
Manufacturer

Atlantic Design Inc.

11505 Pocomoke Court
Baltimore, MD 21220
Contact: Russell Roden
Phone: 866-225-5234
info@calladi.com
www.atlanticdesigninc.com
Manufacturer

Axxiom Manufacturing

11927 S. Highway 6
Fresno, TX 77545
Contact: Sales
Phone: 832-295-5200
sales@axxiommfg.com
www.schmidtabrasiveblasting.com
Manufacturer

Equipment Company Profiles

B

Barton International

Six Warren Street
Glens Falls, NY 12801
Phone: 800-741-7756
info@barton.com
www.barton.com
Manufacturer / Distributor

Beardsley Sales

4535 State Route 89
Seneca Falls, NY 13148
Contact: Dave Swenson
Phone: 315-549-2627
Dswenson@rochester.rr.com
Manufacturer

Bell & MacKenzie Company Ltd.

500 Sherman Ave. P.O. Box 844,
LCD #1
Hamilton, ON L8N 3N9 Canada
Contact: Richard Bell
Phone: 888-794-5665
info@bellandmackenzie.com
Distributor

Bellemare Abrasives&

Minerals(SDF Abrasives, Inc.)

8750 Boul. Industriel
Trois Rivières, QC G9A 5E1 Canada
Contact: Allain Hache/Martin Cote
Phone: 506-380-4017 or
819-376-4366
mcote@groupebellemare.com
www.groupebellemare.com
Manufacturer

Bittner's Spray Equipment Co.

1301 Brummel Avenue
Elk Grove Village, IL 60007
Contact: Greg Bittner
Phone: 847-364-7661
zbitt@msn.com
www.BSEsprayit.com
Distributor

Bix Manufacturing Company, Inc

108 Cude Lane
Madison, WA 37115
Contact: Neheeh Kehrrri
Manufacturer

Blasting Experts

241 West 16th St
Hamilton, ON L9C4C7 Canada
Contact: Eng. Mauricio Herrera
Phone: 905-297-5515
sales@blastingexperts.com
www.blastingexperts.com
Manufacturer / Distributor / Rental
Company

Blastlink USA

11927 Windfern Road
Houston, TX 77064
Contact: Jeanne Haner
blastlink.usa@gmail.com
Distributor

Blastman Robotics Ltd.

Kaarnatie 40
Oulu, 90530 Finland
Contact: Sakari Veijola
Phone: 358-407616561
sakari.veijola@blastman.fi
www.blastman.fi
Manufacturer

BlastOne International

4510 Bridgeway Avenue
Columbus, OH 43219
Contact: Gavin Gooden
Phone: 614-476-3000
sales@blastone.com
www.blastone.com
Distributor / Rental Company

BlastPro Mfg., Inc.

6021 Melrose Lane
Oklahoma City, OK 73127
www.blastpromfg.com

Blastrac

13201 North Santa Fe Ave.
Oklahoma City, OK 73114
Contact: Customer Service
Phone: 800-256-3440
info@blastrac.com
www.blastrac.com
Manufacturer

BlueGreen Technologies LLC

1408 Hamlin Ave., Unit A
Saint Cloud, FL 34771
Contact: Craig Grason
Phone: 407-466-4427
craig@farrow4u.com
www.farrow4u.com
Distributor

Bolair Fluid Handling Systems

17 Brownridge Rd Unit 1&2
Halton Hills - Branch in Alberta and
BC, ON L7G 0C6 Canada
Contact: Gregory Hadow
Phone: 877-326-5247
sales@bolair.ca
www.bolair.ca
Manufacturer / Distributor / Rental
Company

Bon Tool Co.

4430 Gibsonia Rd
Gibsonia, PA 15044
Contact: sales@bontool.com
Phone: 724-443-7080
Manufacturer

Brand Safway

Infrastructure Services Group
Scotia-Glenville Industrial Park
Building 406
Scotia, NY 12302
Contact: Jerry Dolly
Phone: 518-381-6000
quikdeck@safway.com
www.quikdeck.com
Manufacturer / Rental Company

Buffalo Shrink Wrap

PO Box 537
Clarence, NY 14031
Contact: William Casilio Jr
Phone: 716-440-7708
orders@buffaloshrinkwrap.com
www.buffaloshrinkwrap.com
Distributor

Bullard

1898 Safety Way
Cynthiana, KY 41031
Contact: Steve Couture
Phone: 859-234-6616
info@bullard.com
www.bullard.com
Manufacturer

BYK

524 South Cherry Street
Wallingford, CT 06492
Manufacturer

BYK-Gardner USA

9104 Guilford Rd.
Columbia, MD 21046
Contact: Sherry Brown
Phone: 800-343-7721
info.byk.gardner.usa@altana.com
www.byk.com/instruments
Manufacturer

C

Carlisle Fluid Technologies-Binks

16430 N. Scottsdale Rd. Suite 450
Scottsdale, AZ 85254
Contact: Jim Cardosi
Phone: 630-888-1138
info@carlisleft.com
www.binks.com
Manufacturer

Cate Wyoming Equipment Company, LLC

3002 Conestoga Drive
Gillette, WY 82718
Contact: Randy Hartley
Phone: 307-682-0571
Distributor

CBG Biotech

31075 Solon Industrial Parkway
Solon, OH 44139
Contact: Nancy Isom
Phone: 800-941-9484
info@cbgtechnologies.com
cbgbiochem.com
Manufacturer

Central Texas Equipment

1401 Central Commerce Circle
Pflugerville, TX 78660
Contact: Bob Henry
Phone: 512-442-2371
sales@ctegroup.net
www.ctegroup.net
Distributor

CESCO - Aqua Miser

7251 Cross County Rd.
N. Charleston, SC 29418
Contact: Karen Haun
Phone: 843-760-3000
info@BlastandPaint.com
www.blastandpaint.com
Manufacturer / Distributor / Rental
Company

Chesapeake Specialty Products, Inc.

5055 North Point Blvd.
Baltimore, MD 21219
Contact: Kenneth Sanchez
Phone: 410-388-5055
info@chesprod.com
www.chesprod.com
Manufacturer

CHLOR RID International Inc./

Borchers Americas Inc.

811 Sharon Drive
Westlake, OH 44145
Contact: AZ Office
Phone: 480-821-0039
chlorryd@borchers.com
www.chlor-rid.com
Manufacturer

Cincinnati Color Company

1027 Dalton Street
Cincinnati, OH 45203
Contact: Doug Deifel
Phone: 513-241-1090
ddeifel@cincinnati-color.com
www.cincinnati-color.com
Distributor

CLEARBLAST

706 Old Westtown Road Suite E
West Chester, PA 19382
Contact: Sales
Phone: 888-327-7698
info@clearblast.com
www.clearblast.com
Manufacturer

Clemco Industries Corp.

One Cable Car Drive
Washington, MO 63090
Contact: Customer Service
Phone: 636-239-4300
info@clemcoindustries.com
www.clemcoindustries.com
Manufacturer

Clothes Cleaning Systems

4475 Technology Drive
Wilson, NC 27896
Contact: Sam Bowling
Phone: 252-243-3752
sam@skbowling.com
www.clothescleaningsystems.com
Manufacturer / Distributor

Cold Jet

455 Wards Corner Rd.
Loveland, OH 45140
Contact: Brian Allen
Phone: 513-831-3211
info@coldjet.com
www.coldjet.com
Manufacturer

ColorTec & FORMULATOR

Software
28 Center St.
Clinton, NJ 08809
Contact: J. DeGross
Phone: 908-735-2248
sales@color-tec.com
www.color-tec.com
Manufacturer

Corrosion & Protective Coatings S.A.

Av. Paseo La Castellana 814, Urb. La Castellana
Lima, 33 Peru
Contact: Gina Aliaga
Phone: 51-1-449-2006
galiaga@cpcinstrumentos.com
www.cpcinstrumentos.com
Distributor

Corrosion Specialties Inc.

2221 Northmont Parkway Suite 200
Duluth, GA 30096
Contact: Matt Steinmann
Phone: 770-938-7263
msteinmann@corrosionspec.com
www.corrosionspec.com
Distributor

Crawler

2354 North Lindberg Blvd.
St. Louis, MO 63114
Contact: Mark Chick
Phone: 314-428-4804
mark@crawlerusa.com
www.crawlerusa.com
Manufacturer

CS Unitec, Inc.

22 Harbor Avenue
Norwalk, CT 06850
Contact: Kathy Delaney
Phone: 203-853-9522
www.csunitec.com
Manufacturer

Cygnus Instruments Ltd

Cygnus House, 30 Prince of Wales Road
Dorchester, DT1 1PW United Kingdom
Contact: Graham Haines
Phone: 44-1305-265533
sales@cygnus-instruments.com
www.cygnus-instruments.com
Manufacturer

Cygnus Instruments, Inc.

PO Box 6417
Annapolis, MD 21401
Contact: Rod Sanders
Phone: 410-267-9771
sales@cygnusinstruments.com
www.cygnusinstruments.com
Distributor



Dawson-Macdonald Company

845 Woburn Street
Wilmington, MA 1887
Contact: Mike Stygles
Phone: 978-988-8034
info@dawson-macdonald.com
www.dawson-macdonald.com
Distributor

DeFelsko Corporation

800 Proctor Ave.
Ogdensburg, NY 13669
Contact: Terry LaRue
Phone: 315-393-4450
techsale@defelsko.com
www.defelsko.com
Manufacturer

DeHumidification Technologies, LP

6609 Avenue U
Houston, TX 77011
Contact: Brian Battle
Phone: 713-939-1166
bbattle@rentdh.com
www.rentdh.com
Rental Company

Dehumidifiers, Sales and Consulting, Inc.

4319 Brook Shadow Dr.
Kingwood, TX 77345
Contact: Don Bechtol
Phone: 713-249-1615
dbechtol@dhsalesandconsulting.com
www.dhsalesandconsulting.com
Distributor

Desco Manufacturing Company, Inc.

23031 Arroyo Vista
Rancho Santa Margarita, CA 92688
Contact: Ralph Fabian
Phone: 800-337-2648
info@descomfg.com
www.descomfg.com
Manufacturer

Desmond Mfg. Co.

PO Box 30
Urbana, OH 43078
Contact: Robert McConnell
Phone: 937-653-7181
desmondmfg@ctcn.net
www.swirloff.com
Manufacturer

Detroit Tarp, Inc.

6760 Metroplex Dr.
Romulus, MI 48174
Contact: Dennis Trezona
Phone: 800-457-5054
dennistrezona@hotmail.com
www.detroittarp.com
Manufacturer

DevWave Software Inc

PO Box 28031
Victoria, BC V9B 6K8 Canada
Contact: Michael Brown
Phone: 888-739-4033
sales@devwave.com
www.devwave.com
Manufacturer

Diamond Scaffold

2355 Hurricane Bay Dr.
Semmes, AL 36575

Dickson Industries, Inc.

PO Box 684
Tecumseh, OK 74873
Contact: Wayne Dickson
Phone: 405-598-6547
dicksonparts@aol.com
www.roadproonline.com
Manufacturer

Diedrich Technologies Inc.

310 Wayto Road
Schenectady, NY 12303
Contact: Ken Eglin
Phone: 800-283-3888
moreinfo@sandellmfg.com
www.diedrichtechnologies.com
Manufacturer

Disnamair, S.A.

Jose Picon, 18
Madrid, 28028 Spain
Contact: Carlos Aguirre
Phone: 34-913611051
carlos@disnamair.com
www.disnamair.com
Distributor

Dispensing Technology Corporation

5500 Adolfo Road
Camarillo, CA 93012
Contact: Todd White
Phone: 805-388-5575
sales@dispensingtech.com
www.dispensingtech.com
Manufacturer

Doosan Portable Power

1293 Glenway Drive
Statesville, NC 28625
Phone: 800-633-5206
portablepowersales@doosan.com
www.doosanportablepower.com
Manufacturer

Draygon LLC

313 Seaboard Avenue
Venice, FL 34285
Contact: Raymond E. VanKouwenberg
Phone: 585-329-9718
ray@draygon.com
www.draygon.com
Manufacturer

Dry Air Technology

313 North Oak St.
Burlington, WA 98233
Contact: Lori Buswell
Phone: 360-755-9176
info@dryairtech.com
www.dryairtech.com
Manufacturer

Equipment Company Profiles

DryAIR by TDM

52 US Route 1 #2
Scarborough, ME 04074
Contact: Mark Callahan
Phone: 800-287-1538
mcallahan@tdmgo.com
www.tdmgo.com
Manufacturer

DuPont Protection Solutions

PO Box 27001
Richmond, VA 23261
Contact: DuPont Personal
Protection Customer Service
Phone: 800-931-3456
personalprotection.dupont.com
www.safespec.dupont.com
Manufacturer

Dustless Blasting

5711 Schurmier Rd.
Houston, TX 77048

Dustless Technologies

1285 E. 650 South
Price, UT 84501
Contact: Cameron Jaccard
Phone: 435-637-5885
orders@dustlesstools.com
www.dustlesstools.com
Manufacturer

DUX Technologies, Inc.

PO Box 1314
Seahurst, WA 98062
Contact: Brad Rice
Phone: 206-248-0808
brad.rice@dutextechnologiesinc.com
www.dutextechnologiesinc.com
Manufacturer

E

Eagle Industrial Equipment, Inc.

230 N. Barrios St.
Lockport, LA 70374
Contact: Ben Ledet
Phone: 800-621-1511
bledet@eagleie.com
www.eagleie.com
Manufacturer

Eagle Industries

PO Box 10652
New Orleans, LA 70123
Contact: Patrick Calvo
Phone: 800-266-8246
patrick@eagleind.com
www.eagleind.com
Manufacturer

ECSS

6082 Anna Ct.
Eastvale, CA 92880
Contact: Eric Villaseñor
Phone: 909-952-0745
eddycurrentguru@aol.com
www.eddycurrentandcoatingsales.com
Distributor

Eco-Shell, Inc.

5230 Grange Road
Corning, CA 96021
Contact: Helen Cantrell
Phone: 530-824-8794
sales@ecoshell.com
www.ecoshell.com
Manufacturer

ECS North America, LLC

148 Mill Rock Road East
Old Saybrook, CT 06475
Contact: Erin Bogan
Phone: 860-395-4760
erin@ecsone.com
www.ecsone.com
Rental Company

Elcometer (Asia) Pte Ltd

896 Dunearn Road, Sime Darby
Centre, #03-09
Singapore, 589472 Singapore
Contact: Andy Foo
Phone: 656-462-2822
andy@elcometer.com.sg
www.elcometer.com.sg
Distributor

Elcometer, Inc.

1893 Rochester Industrial Drive
Rochester Hills, MI 48309
Contact: Sunny Nietubicz
Phone: 800-521-0635
sales@elcometerusa.com
www.elcometerusa.com
Manufacturer / Distributor

ElektroPhysik Dr. Steingroever GmbH & Co. KG

Pasteurstr. 15
Cologne, D-50735 Germany
Contact: Sales Dept.
Phone: 49-221-752040
info@elektrophysik.com
www.elektrophysik.com
Manufacturer / Distributor

EnDiSys

14329 Northdale Blvd.
Rogers, MN 55374
Contact: Scott L. Striggow
Phone: 763-428-5075
scottstriggow@endisys.com
www.endisys.com
Manufacturer / Distributor

ENMET

680 Fairfield Ct.
Ann Arbor, MI 48108
Contact: ENMET Customer Service
Phone: 800-521-2978
rkelley@enmet.com
www.enmet.com
Manufacturer

EnTech Industries

1109 10th St. NE
East Grand Forks, MN 56721
Contact: Mark LaPlante
Phone: 218-773-6602
mark@entechindustries.com
www.entechindustries.com
Manufacturer

Enviro-Prep System - a product of hci

310 S. Bellis St.
Wausau, WI 54403
Contact: Rachel Rohland
Phone: 715-845-7221
info@enviro-prep.com
www.enviro-prep.com
Manufacturer

Envirosafe Stripping Inc.

785 Arch Street
Carnegie, PA 15106
Contact: Mike Vorel
envirosafeindustrial@verizon.net
www.envirosafeindustrial.com
Manufacturer

Epic Minerals LLC

1260 Hawthorne Ridge Dr.
Brookfield, WI 53045
Contact: Tim Nechvatal
Phone: 414-331-6570
epicminerals@gmail.com
www.epicminerals.com
Distributor

EPIC Supply, LLC

45 Whitestone Lane
Lancaster, NY 14086

Equipment Development Co., Inc.

100 Thomas Johnson Drive
Frederick, MD 21702
Contact: Ray Tucker
Phone: 800-638-3326
sales@edcoinc.com
www.edcoinc.com
Manufacturer

Ervin Industries, Inc.

3893 Research Park Dr.
Ann Arbor, MI 48106
Contact: Joe McGreal
Phone: 800-748-0055
jmcgreal@ervinindustries.com
www.ervinindustries.com
Manufacturer

ESCA Blast

1330 Industry Road
Hatfield, PA 19440
Contact: Ed Swayze
Phone: 215-723-9000
www.escablast.com
Distributor / Rental Company

Everblast Inc.

820 McArdle Drive, Unit C
Crystal Lake, IL 60014
Contact: Chris Hindley
Phone: 815-788-8660
sales@everblast.com
www.everblast.com
Manufacturer

ExakTime

27001 Agoura Rd. Suite 280
Calabasas, CA 91301
Contact: Anthony Alexandre
Phone: 818-334-2576
anthony.alexandre@exaktime.com
www.exaktime.com
Manufacturer

F

Faulks Bros.

E 3481 Hwy 22 & 54
Waupaca, WI

Fehr Bros. Industries, Inc.

895 Kings Hwy.
Saugerties, NY 12477
Contact: Paul Stauble
Phone: 800-431-3095
pstauble@fehr.com
www.fehr.com
Distributor

Fischer Technology, Inc.

750 Marshall Phelps Rd.
Windsor, CT 06095
Contact: Geoff Koehn / Juliann
Goodwill
Phone: 860-298-6060
sales@fischer-technology.com
www.fischer-technology.com
Manufacturer

Equipment Company Profiles

Flashlights Unlimited

416 Mapmaker Ln
Savannah, GA 31410
Contact: Floyd Hacker
Phone: 912-999-6378
floyd@flashlightsunlimited.com
www.flashlightsunlimited.com
Manufacturer / Distributor

Flat Rock Bagging

27938 Cooke St
Flat Rock, MI 48134
Contact: Mike Simonetti
Phone: 734-782-2073
mikesim@flatrockbagging.com
www.flatrockbagging.com
Manufacturer / Distributor

Flexible Lifeline Systems

14325 West Hardy Rd.
Houston, TX 77060
Contact: Sales
Phone: 832-448-2900
info@flexiblelifeline.com
www.flexiblelifeline.com
Manufacturer

Floorex Products

11-13 Jennings Road
Swan Hill, 3585 Australia
Contact: Sales Team
Phone: 61-3-5036-4000
sales@floorex.com.au
www.floorex.com
Manufacturer

Franmar

PO Box 5565
Bloomington, IL 61701
Contact: Customer Service
Phone: 800-538-5069
custserv@franmar.com
www.franmar.com
Manufacturer / Distributor

Friess Equipment, Inc.

2222 Akron-Peninsula Rd.
Akron, OH 44313
Contact: Jim Friess
Phone: 330-945-9440
friessequipment@sbcglobal.net
Manufacturer / Distributor

FROHN North America Inc.

6289 Bankhead Hwy., Bldg. 11 A-D
Austell, GA 30168
Contact: Jed Palmer
Phone: 877-362-7336
jed.palmer@frohn.us
www.frohn.com
Manufacturer

FS Solutions

1144 Expressway Drive South
Toledo, OH 43608
Contact: Craig Aspinall / David Brown
Phone: 888-415-4368
rentals@fssolutionsgroup.com
www.fssolutionsgroup.com
Rental Company



Gaco Western

200 W Mercer St., Suite 202
Seattle, WA 98119
Contact: Customer Service
Phone: 800-331-0196
customerservice@gaco.com
www.gaco.com
Manufacturer

GAL Power Systems Toronto

217 Statesman Drive
Mississauga, ON L5S 1X4 Canada
Contact: Mr. Dustin Hubert
Phone: 855-563-7847
d.hubert@galpower.com
www.galpower.com
Rental Company

Galeton Gloves and Safety Products

PO Box 336
Mansfield, MA 02048
Contact: Bill Forbes
Phone: 800-221-0570
galeton.com
Distributor

GapVax Inc.

575 Central Avenue
Johnstown, PA 15902
Contact: Matt Hughes
Phone: 814-535-6766
mhughes@gapvax.com
www.gapvax.com
Manufacturer

GBS Scaffolding and Services Corp.

38750 Webb Dr., Ste. 100
Westland, MI 48185
Contact: Steve Fenske
Phone: 888-868-1062
gbsscaffolding@gmail.com
www.gbsscaffolding.com
Manufacturer / Distributor / Rental Company

General Lasertronics Corporation

830 Jury Court, Suite 5
San Jose, CA 95112
Phone: 408-947-1181
info@lasertronics.com
www.lasertronics.com
Manufacturer

General Pump

1174 Northland Drive
Mendota Heights, MN 55120
Contact: Joe Campbell
Phone: 888-474-5487
sales@gpcompanies.com
www.generalpump.com
Manufacturer

Glenn Saren & Assoc. Inc.

8460 NW 52nd Pl.
Coral Springs, FL 33067
Contact: Glenn Saren
Phone: 305-613-9323
gesaren@aol.com
www.glennsarenassoc.net

GLOBAL Encasement, Inc.

701 E. Santa Clara St.
Ventura, CA 93001
Contact: George C. Keefe
Phone: 800-266-3982
service@encasement.com
www.encasement.com
Manufacturer

GMA Garnet (Europe) GmbH UK Office

P.O. Box 9
Middlewich, CW10 9FD United Kingdom
Contact: Mike Crowe
Phone: 773-863-8966
sales@gmagarnet.co.uk
www.gmagarnet.co.uk
Manufacturer

GMA Garnet (USA) Corporation

1800 Hughes Landing Blvd. Suite 350
The Woodlands, TX 77380
Contact: Pete Mitchell
Phone: 832-243-9300
petem@gmaamericas.com
www.garnetsales.com
Manufacturer / Distributor

Goff, Inc.

12216 NS 3520
Seminole, OK 74868
Contact: David Zehren
Phone: 405-278-6200
goff@goff-inc.com
www.goff-inc.com
Manufacturer

Graco Inc.

88 - 11th Ave. NE
Minneapolis, MN 55413
Contact: Courtney Beall
Phone: 612-208-5654
courtney_a_beall@graco.com
www.graco.com
Manufacturer

Green Diamond Sand Products

PO Box D
Riddle, OR 97469
Contact: Kennette Wilson
Phone: 541-874-3111
kwilson@greendiamondsand.com
www.greendiamondsand.com
Manufacturer

Greener Blast Technologies, Inc.

73 Progress Ave.
Tyngsboro, MA 01879
Contact: info@greenerblast.com
Phone: 978-649-5300
Info@greenerblast.com
greenerblast.com
Manufacturer

Gritco Equipment B.V.

Klompemakerstraat 16D
Ridderkerk, NL-2984 BB
Netherlands
Contact: Sander van der Made
Phone: 31-180-412855
info@gritco.com
www.gritco.com
Manufacturer / Distributor

Guzzler Manufacturing

1621 S. Illinois Street
Streator, IL 61364
Contact: Nick Bruhn
Phone: 815-672-3171
sales@guzzler.com
www.guzzler.com
Manufacturer



Hammelmann Corp.

436 Southpointe
Miamisburg, OH 45342
Contact: Ray Oetzel
Phone: 937-859-8777
mail@hammelmann.com
www.hammelmann.com
Manufacturer

Equipment Company Profiles

Hammelmann GmbH

Carl-Zeiss-Str. 6-8
Oelde, 59302 Germany
Contact: Matthias Knoedler
Phone: 49-2522760
sales@hammelmann.de
www.hammelmann.com
Manufacturer

Hanes Supply Inc

55 James E Casey Drive
Buffalo, NY 14206
Contact: Eric Kuras
Phone: 716-826-2636
sales@hanessupply.com
www.hanessupply.com
Manufacturer / Distributor / Rental Company

Harsco

350 Popular Church Road
Camp Hill, PA 17010
Contact: Customer Service
Phone: 888-733-3646
reedcs@harsco.com
www.blackbeautyabrasives.com
Manufacturer

Hartzell Air Movement

910 S. Downing Street
Piqua, OH 45356
Contact: Local sales rep
Phone: 937-773-8494
info@hartzell.com
www.hartzell.com
Manufacturer

Hawk Research Labs

780 A.E.C. Drive
Wood Dale, IL 60191

HERO Products Group a division of I.C.T.C. Holdings Corp.

720 Eaton Way
Delta, BC V3M 6J9 Canada
Contact: Steve Babins
Phone: 604-523-3080
sbabins@hero.ca
www.hero.ca
Manufacturer

Hertz Equipment Rental

74-591 Honokohau St.
Kailua-Kona, HI 96740
Contact: Bobby Marks
Phone: 808-331-1304
Distributor

HoldTight Solutions

PO Box 27907
Houston, TX 77227
Contact: Ken Rossy
Phone: 832-633-0430
ken.rossy@holdtight.com
www.holdtight.com
Manufacturer / Distributor

Honeywell Safety Products

900 Douglas Pike
Smithfield, RI 02917
Contact: Mike Bennett
Phone: 513-703-9486
michael.bennett2@honeywell.com
www.honeywellsafety.com
Manufacturer

HoverTrowel, Inc.

5048 Spruce Lane
Mohnton, PA 19540
Contact: Eric Kuras
Phone: 610-856-1961
sales@hovertrowel.com
www.hovertrowel.com
Manufacturer

Hyde Group

54 Eastford Road
Southbridge, MA 01550
Contact: Customer Service
Phone: 800-872-4933
custrelations@hydetools.com
www.hydetools.com
Manufacturer

IBIX North America, Surface Tech. LLC

2075 Lake Ave. NE
Largo, FL 33771
Contact: sales@ibixusa.com
Phone: 727-322-4611
sales@ibixusa.com
www.ibixusa.com
Distributor

ICM - International Climbing Machines

630 Elmira Road
Ithaca, NY 14850
Contact: Samuel Maggio
Phone: 607-288-4001
info@icm.cc
www.icm.cc
Manufacturer

IDS Blast

2717 Tobey Dr.
Indianapolis, IN 46219
Contact: John Heinzelman
Phone: 800-800-0665
johnh@idsblast.com
www.idsblast.com
Distributor

IKK Shot Co., Ltd. - Japan

412-4 Nunowari, Minami Shibata
Machi
Tokai, Aichi, 476-0001 Japan
Contact: Customer Service
Phone: 81-52-307-8100
contact.japan@wabrasives.com
www.wabrasives.com

INDCO, Inc.

4040 Earnings Way
New Albany, IN 47150
Contact: Tricia Thien
Phone: 800-942-4383
info@indco.com
www.indco.com
Manufacturer

Indian Valley Industries, Inc.

5 Pine Camp Drive
Binghamton, NY 13904
Contact: Cord Pennell
Phone: 607-240-8407
cpennell@iviindustries.com
www.iviindustries.com
Manufacturer

Industrial Mineral Co.

1/1C Harbour Express Highway
Road, Thermal Nagar I,
Tuticorin
Tuticorin, Tamilnadu, 628006 India
Contact: Madhavan.K.
Phone: 91-461-2383001
madhavan@industrialmineral.in
www.industrialmineral.in
Manufacturer

Industrial Vacuum Equipment Corp.

N8150 Maple Street
Ixonia, WI 53036
Contact: Randy Bourdo
Phone: 800-331-4832
randy@industrialvacuum.com
www.industrialvacuum.com
Manufacturer

Innovative Reach

5505 Twin Knolls Dr
Cedar Rapids, IA 52411
Contact: Philip Koch
Phone: 319-573-3488
info@innovativereach.com
www.innovativereach.com
Rental Company

Intech Equipment & Supply

1921 W Grant St
Phoenix, AZ 85009
Contact: John Linn
Phone: 602-909-6822
johnl@intechequipment.com
www.intechequipment.com
Distributor



J.D. Honigberg International, Inc.

155 North Pfingsten Road, Suite 150
Deerfield, IL 60015
Contact: Javier Guerrero
Phone: 224-804-6015
jguerrero@jdhintl.com
www.jdhpowerequipment.com
Distributor

Jadalc

Calle los Nazcas, N 231 Urb.
Maranga San Miguel
Lima, L-32 Peru
Contact: Jose Antonio De Amat
Lacotera
Phone: 99-9976634
deamat@waterjetting.com.pe
www.waterjetting.com.pe
Distributor

James Instruments Inc.

3727 N. Kedzie Ave.
Chicago, IL 60618
Contact: Michael W. Hoag
Phone: 773-463-6565
773-463-6565
www.ndtjames.com
Manufacturer

Jenny Products, Inc.

850 North Pleasant Ave.
Somerset, PA 15501
Contact: Dan Leiss
Phone: 888-425-3669
info@jennyproductsinc.com
www.jennyproductsinc.com
Manufacturer

Jet Edge

12070 43rd St. NE
St. Michael, MN 55376
Contact: Barb Trushenski
Phone: 763-497-8700
sales@jetedge.com
www.jetedge.com
Manufacturer

Jetstream of Houston

5905 Thomas Road
Houston, TX 77041
Contact: Ron Felts
Phone: 832-590-1300
sales@waterblast.com
www.waterblast.com
Manufacturer

Jollyflex

Rubber Park, Valayanchirangara
Ernkulam, Kerala, 683556 India
Phone: 91-484-2655135
info@jollyflex.net
www.jollyflex.net
Manufacturer / Distributor

Julbert, Inc.

476 Shannon Lane
Priest River, ID 83856
Contact: Robert Fhuere
Phone: 208-448-4440
customerservice@julbertinc.com
www.julbertinc.com
Manufacturer / Distributor / Rental
Company

K

Kee Safety

100 Stradtman Street
Buffalo, NY 14206
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info@keesafety.com
www.keesafety.com
Manufacturer

Kennametal Inc.

2879 Aero Park Drive
Traverse City, MI 49686
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k-trvr.service@kennametal.com
www.kennametal.com
Manufacturer

Khushboo Scientific Pvt. Ltd.

132 Princess Street, Govind
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Mumbai, 400 002 India
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sales@khushbooscientific.com
www.khushbooscientific.com
Distributor

Kovobrasiv (CZ)

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Brdy, Czech Republic
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Phone: 420-318-533-037
contact.czech-republic@
wabrasives.com
www.wabrasives.com

KS International, Inc.

PO Box 8835
Greenville, SC 29604
Contact: Nancy Hamilton
Phone: 864-370-9744
cleansafe@dropcloth.com
www.dropcloth.com
Distributor

KTA-Tator, Inc.

115 Technology Drive
Pittsburgh, PA 15275
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Phone: 412-788-1300
mfajt@kta.com
www.ktagage.com
Distributor

L

Lesoon Equipment Pte. Ltd.

81, Tuas South Street 5
Singapore, 637651 Singapore
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Phone: 65-67902900
enquiry@lesoon.com.sg
www.lesoon.com.sg
Manufacturer / Distributor

Lignomat USA Ltd

14345 NE Morris Ct.
Portland, OR 97230
Contact: Grete Heimerdinger
Phone: 800-227-2105
sales@lignomat.com
www.lignomat.com
Manufacturer

Lisbon Hoist, Inc.

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Lisbon, OH 44432
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Phone: 330-424-7283
connie@lisbonhoist.com
www.lisbonhoist.com
Manufacturer

LPI Incorporated

4404 Anderson Drive
Eau Claire, WI 54703
Contact: Ardy Robertson
Phone: 800-657-6956
sales@lpi-inc.com
www.lpi-inc.com
Manufacturer

LS Industries, Inc.

710 E. 17th
Wichita, KS 67214
Contact: Roger Carvalho
Phone: 316-265-7997
sales@lsindustries.com
www.lsindustries.com
Manufacturer

M

Magnolia Brush

1001 N. Cedar St.
Clarksville, TX 75426
Contact: Glenn Guyette
Phone: 800-248-2261
sales@magnoliabrush.com
www.magnoliabrush.com
Manufacturer

Manus Abrasive Systems, Inc./

Mod-U-Blast Mfg.
1040 - 78 Avenue
Edmonton, AB T6P 1L7 Canada
Contact: Robin T. MacLean
Phone: 780-468-2588
macleanr@manusabrasive.com
www.modublast.com
Manufacturer / Distributor / Rental
Company

Marco

3425 East Locust Street
Davenport, IA 52803
Contact: Marco
Phone: 800-252-7848
sales@marco.us
www.marco.us
Manufacturer / Distributor / Rental
Company

The Marindus Company, Inc.

PO BOX 663
Englewood, NJ 7631
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info@marindusco.com
www.marindusco.com
Manufacturer / Distributor / Rental
Company

Masterfield Industrial Equipment

17 Stanley Street
Silverwater NSW, 2128 Australia
Contact: Elicia Thornhill
Phone: 61-2-9193-9000
sales@masterfield.com.au
www.masterfield.com.au
Manufacturer / Distributor

Mattson Spray Equipment

230 W. Coleman St.
Rice Lake, WI 54868
Contact: Paul Lenzen
Phone: 800-877-4857
mse@mattsonspray.com
www.mattsonspray.com
Manufacturer / Distributor

McClung-Logan Equipment Co.

4601 Washington Blvd.
Baltimore, MD 21227
Contact: James Reid
Phone: 401-242-6500
jreid@mcclung-logan.com
www.mcclung-logan.com
Distributor

MES Rentals

32128 Broken Branch Circle
Spanish Fort, AL 36527
Contact: Chris Keenan
Phone: 888-281-2643
sales@mesrentals.com
www.mesrentals.com
Manufacturer / Distributor / Rental
Company

Metabrase (UK)

Ironmasters Way
Stillington, TS21 1LE United
Kingdom
Contact: Customer Service
Phone: 44-1740-632-100
contact.united-kingdom@
wabrasives.com
www.wabrasives.com
Manufacturer

Metal Samples

152 Metal Samples Rd.
Munford, AL 36268
Contact: Brenda Smith
Phone: 256-358-4202
msc@alspi.com
www.metalsamples.com
Manufacturer

Michigan Ladder Co.

12 East Forest Avenue P.O. Box
981307
Ypsilanti, MI 48198
Contact: Bob Hoernschemeyer
Phone: 734-482-5946
bobh@michiganladder.com
www.michiganladder.com
Manufacturer

Midwest Mobile Waterjet

555 Bardge Channel Road
Saint Paul, MN 55104
Contact: Brian Gleeson
Phone: 651-755-7089
bgleeson@mmwaterjet.com
www.mmwaterjet.com
Manufacturer

Equipment Company Profiles

Midwest Surface Prep, LLC

PO Box 78551
Indianapolis, IN 46268
Contact: Sales Manager
Phone: 317-250-4734
quote@midwestafi.com
www.midwestsurfaceprep.com
Distributor

Minerals Research, Inc.

4620 South Coach Dr.
Tucson, AZ 85714
Contact: Mike McLouth
Phone: 520-297-4626
mike.mclouth@mineralsresearch.com
www.mineralsresearch.com
Manufacturer

Mobile Abrasives Inc

6927 Mac Drive
Theodore, AL 36582
Contact: Matt Serda
Phone: 251-694-0023
www.mobileabrasives.com
Manufacturer

MONTI Tools Inc.

10690 Shadow Wood Drive, Suite 113
Houston, TX 77043
Contact: info@monti-tools.com
Phone: 832-623-7970
info@monti-tools.com
www.monti-tools.com
Manufacturer

Montipower, Inc.

7677 Coppermine Dr.
Mannassas, VA 20109
Contact: Charles Lockard
Phone: 703-396-8777
clockard@mbxit.com
www.mbxit.com
Distributor

Mr. Shrinkwrap

PO Box 697
Media, PA 19063
Contact: Kevin Comerford
Phone: 610-566-5290
kevc@mrshrinkwrap.com
www.mrshrinkwrap.com
Distributor

MSA

1000 Cranberry Woods Dr
Cranberry Twp, PA 16066
Contact: Inside Sales
Phone: 800-672-9010
msainsidesales@msasafety.com
www.msasafety.com
Manufacturer

MST, Inc. (Modern Safety Techniques)

11370 Breininger Rd., PO Box 87
Hicksville, OH 43526
Phone: 800-542-6646
sales@modsafe.com
www.modsafe.com
Manufacturer

Munters Corporation

79 Monroe Street
Amesbury, MA 01913
Contact: Courtney Tyler
Phone: 978-241-1100
dhinfo@munters.com
www.munters.com
Manufacturer

N

N.T. Ruddock Co.

26123 Broadway Ave.
Cleveland, OH 44146
Contact: Jim Ruddock
Phone: 440-439-4976
sales@ntruddock.com
www.ntruddock.com
Distributor

National Concrete Accessories

172 Bethridge Road
Toronto, ON M9W 1N3 Canada
Contact: Steve Kekewich
Phone: 416-245-4720
sales@nca.ca
www.nca.ca
Manufacturer / Distributor

Nationwide Overspray

P.O. Box 810513
Dallas, TX 75381
Phone: 972-243-8882
www.nationwideoverspray.com/
Distributor

Natrium Products, Inc.

58 Pendleton Street PO Box 5465
Cortland, NY 13045
Contact: Tim Herman
Phone: 800-962-4203
herman@natrium.com
www.natriumsodablast.com
Manufacturer

NDT Systems

5542 Buckingham Dr
Huntington Beach, CA 92649
Contact: Greg Smith
Phone: 877-455-4638
sales@ndtsystems.com
www.ndtsystems.com
Manufacturer

Nelson Industrial Services

6021 Melrose Lane
Oklahoma City, OK 73127
Contact: Paul Jackson
Phone: 405-495-9797
pjackson@nelsonindustrial.com
www.nelsonindustrial.com
Manufacturer

The New York Blower Company

7660 Quincy St.
Willowbrook, IL 60527
Phone: 800-208-7918
nyb@nyb.com
www.nyb.com
Manufacturer

Newstripe

1700 Jasper Drive Unit F
Aurora, CO 80011
Contact: Shawn Hunter
Phone: 303-364-7786
info@newstripe.com
www.newstripe.com
Manufacturer

NGF Canada Limited

Glass Flake Coatings Additives
Division 255 York Road
Guelph, ON N1E 3G4 Canada
Contact: Ed Malison
Phone: 519-835-6422
ed.malison@ngfcanada.com
www.microglas.com and
www.metalshine.com
Manufacturer

NLB Corp.

29830 Beck Road
Wixom, MI 48393
Contact: Andrew Chilkiewicz
Phone: 248-624-5555
nlbmktg@nlbusa.com
www.nlbcorp.com
Manufacturer / Rental Company

Norton Sandblasting Equipment

1006 Executive Blvd.
Chesapeake, VA 23320
Contact: Jason Eisel
Phone: 757-548-4842
info@nortonsandblasting.com
www.nortonsandblasting.com
Distributor / Rental Company

Nour Trading House Inc.

637 Colby Dr.
Waterloo, ON N2V1B4 Canada
Contact: Nour Fleifel
Phone: 226-929-2064
nourf@nour.com
www.nour.com
Manufacturer

Novatek Corporation

700 Schell Lane
Phoenixville, PA 19460
Contact: Sales Department
Phone: 610-363-7800
sales@novatekco.com
www.novatekco.com
Manufacturer

NTI Global

50 Willow St.
Amsterdam, NY 12010
Contact: Sarek Raeburn
Phone: 800-947-7767
sarek@ntiglobal.com
www.ntiglobal.com
Manufacturer

Nueces Power Equipment

PO Box 4789
Corpus Christi, TX 78469
Contact: Wes Danklefs
Phone: 361-289-0066
Distributor

Nueces Power Equipment

4501 US Hwy. 59
Victoria, TX 77905
Phone: 361-576-0066
Distributor

Nueces Power Equipment

5220 Expwy. 281S
Edinburg, TX 78539
Contact: Edward Dominguez
Phone: 956-702-0066
ednpowernequip@att.net
www.nuecespower.com
Distributor

Equipment Company Profiles

Nueces Power Equipment

One Industrial Way
San Benito, TX 78586
Contact: Robert Zohrer
Phone: 956-361-0066
Distributor

Nueces Power Equipment

8241 S Desert Blvd
Vinton, TX 79821
Contact: Steve Donnelly
Phone: 915-541-0066
Distributor

NZ Corrosion Services Ltd.

751 Carrington Rd. RD1
New Plymouth, 4371 New Zealand
Contact: Sales@corrosion.co.nz
Phone: +64 6 7581745
Sales@corrosion.co.nz
www.corrosion.co.nz
Rental Company



Oak Ridge Foam and Coating Systems

575 Commercial Ave
Green Lake, WI 54941
Contact: Rich Franklin
Phone: 800-625-9577
richf@oakridgepoly.com
www.oakridgepoly.com
Manufacturer / Distributor

Opta Minerals Inc.

407 Parkside Drive, PO Box 260
Waterdown, ON LOR 2H0 Canada
Contact: Customer Service
Phone: 800-743-0094
info@optaminerals.com
www.optaminerals.com
Manufacturer / Distributor

Opti-Blast

4032-B N. Jackson
Jacksonville, TX 75766
Contact: Chris Howard
Phone: 903-589-0452
choward@optiblast.com
www.optiblast.com
Manufacturer



Pacific Roller Die Company, Inc.

1321 W. Winton Avenue
Hayward, CA 94545
Contact: Michael Kraut
Phone: 510-782-7242
michael@prdcompany.com
www.prdcompany.com
Manufacturer

Paint Brush Corporation

27 West Cherry St., PO Box 371
Vermillion, SD 57069
Contact: Jill VonEhwegen
Phone: 800-843-9930
jill@paintbrushcorp.com
www.paintbrushcorp.com
Manufacturer

The Paint Project, Inc.

71 West Street
Medfield, MA 02052
Contact: Bob Zaffino
Phone: 508-359-8003
bob@paintproject.com
www.paintproject.com
Distributor / Rental Company

Panblast Pte Ltd

2 Woodlands Sector 1 #5-06
Woodlands Spectrum I
Singapore, 738068 Singapore
Contact: Garry Simmons
Phone: 65-6586-1583
inquiries@panblast.com
www.panblast.com
Manufacturer

Pangborn

4630 Coates Drive
Fairburn, GA 30213
Contact: Greg Bowers
Phone: 800-638-3000
info@pangborn.com
www.pangborn.com
Manufacturer

Paul N. Gardner Co., Inc.

316 NE 1st St.
Pompano Beach, FL 33060
Contact: Jim Wick
Phone: 954-946-9454
gardner@gardco.com
www.gardco.com
Manufacturer / Distributor

PCWI International Pty. Ltd.

13 Alhambra Ave.
Cardiff, 2285 NSW Australia
Contact: Mark Clark
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sales@pcwi.com.au
www.pcwi.com.au
Manufacturer

Pellets, LLC

63 Industrial Drive
North Tonawanda, NY 14120
Contact: Mike Deakin
Phone: 716-693-1750
mdeakin@pelletslc.com
www.pelletslc.com
Manufacturer / Distributor

Persyst Enterprises, Inc.

4695 Melvin St.
Las Vegas, NV 89115
Contact: Mike Lawson
Phone: 702-362-9432
mike@solvent-recycler.com
www.solvent-recycler.com
Manufacturer / Distributor

Pinnacle Central Co.

103 Bryan St.
Jacksonville, FL 32202
Contact: Billy Porter
Phone: 904-354-5746
info@pinnaclecentral.com
www.pinnaclecentral.com
Distributor / Rental Company

Pipeline Inspection Company

1919 Antoine Dr
Houston, TX 77055
Contact: Ashlee Rogers
Phone: 713-681-5837
sales@picltd.com
www.picltd.com
Manufacturer / Distributor / Rental Company

Pirate Brand

2719 Tobey Dr.
Indianapolis, IN 46219
Contact: Dave Miller
Phone: 800-692-6223
sales@forecastsalesinc.com
www.pirate-brand.com/
Manufacturer

Polygon US Corporation

15 Sharpners Pond Road, Building F
North Andover, MA 01845
Contact: Summer Street
Phone: 800-422-6379
summer.street@polygongroup.com
www.polygongroup.us
Rental Company

Potters Industries LLC

300 Lindenwood Dr.
Malvern, PA 19355
Contact: Mark Shinnars
Phone: 610-651-4652
mark.shinnars@pottersbeads.com
www.pottersbeads.com
Manufacturer

PreTox Products - NexTec, Inc.

4050 Westmark Dr.
Dubuque, IA 52002
Contact: Dave Steffen
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DaveS@PreTox.com
www.pretox.com
Manufacturer

Pro-Am Safety, Inc.

Thorn Hill Ind. Prk., 551 Keystone Dr.
Warrendale, PA 15086
Contact: Michael Arrisher
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mikea@pro-am.com
www.proamsafety.com
Distributor

Pro-Tect Plastic and Supply, Inc.

PO Box 1377
Jacksonville, OR 97530
Contact: Sharri Griffin
Phone: 800-889-9727
sales@pro-TECT.net
www.shrinkwrapcontainments.com
Distributor

Pro-Tect Services, Inc.

12235 Hwy. 105 East
Conroe, TX 77305
Contact: Steve Scott
Phone: 713-589-4638
sales@pro-TECTservices.com
www.pro-TECTservices.com
Distributor

PTQ Safety

8302 Almeda Genoa
Houston, TX 77075
Contact: Julie Todd
Phone: 713-504-8546
julie@ptqsafety.com
www.ptqsafety.com
Manufacturer

Equipment Company Profiles



Q-Lab Corporation

800 Canterbury Road
Westlake, OH 44145
Contact: James Gauntner
Phone: 440-835-8700
info@q-lab.com
www.q-lab.com
Manufacturer

Quikspray, Inc.

PO Box 327
Port Clinton, OH 43452
Contact: Leah Barker
Phone: 419-732-2611
leah@quikspray.com
www.quikspray.com
Manufacturer



Radian's, Inc.

5305 Distriplex Farms Drive
Memphis, TN 38141
Contact: Jon Smith
Phone: 877-723-4267
sales@radians.com
www.radians.com
Manufacturer

Radian's, Inc. Latin America

5305 Distriplex Farms Drive
Memphis, TN 38141
Contact: Juan David Herrera
Phone: 901-388-7776
jd.herrera@radians.com
www.radians.com
Manufacturer

Rapid Deployable Systems

1005 Bankton Circle
Hanahan, SC 29410
Contact: Zeke Lowell
Phone: 843-323-8465
zeke@rapiddeloyablesystems.com
www.rapiddeloyablesystems.com
Manufacturer

Rapid-Prep, LLC

44 Cross Park Ave.
North Kingstown, RI 02852
Contact: Mike Hogue
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sales@rapidprep.com
www.rapidprep.com
Rental Company

RBW Enterprises, Inc.

136 Hillwood Circle
Newnan, GA 30263
Contact: John Vogel or Steve Meyers
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jvogel@rbwe.com
www.rbwe.com
Manufacturer

RCG America

24624 N Interstate 45, Suite 200
Spring, Texas 77389
Contact: Scott Trom
Phone: 281-362-2801
strom@glassox.com
glassox.com

Remote Orbital Installations, LLC

429 Venture Court
Verona, WI 53593
Contact: Michael Kronz
Phone: 608-845-0360
mkronz@roi360.com
www.roi360.com
Manufacturer

Ring Power Corporation

500 World Commerce Parkway
St. Augustine, FL 32092
Contact: Micah Hughes
Phone: 904-494-1285
aircompressor@ringpower.com
www.compressedair.ringpower.com
Distributor / Rental Company

Robovent

37900 Mound Rd.
Sterling Heights, MI 48310
Contact: Trevor Hewitt
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trevor.hewitt@robovent.com
www.robovent.com
Manufacturer

Rodeco Company

5811 Elwin Buchanan Drive
Sanford, NC 27330
Contact: Mark Lawrence
Phone: 800-849-0871
mark.lawrence@rodeco.com
www.rodeco.com

RPB Safety

2807 Samoset Road
Royal Oak, MI 48073
Contact: Kurt Ivory
Phone: 866-494-4599
kurt.ivory@rpbafety.com
www.rpbafety.com
Manufacturer

RPR Technologies AS

Nedre Kongerod 47
Skien, 3737 Norway
Contact: Tom Arne Baann
Phone: 47-91151007
info@rprtech.com
www.rprtech.com
Manufacturer

RUSTECO LLC

PO Box 11398
Torrance, CA 90510
Contact: Michael
Phone: 800-787-8326
rusteco@aol.com
www.rusteco.com
Manufacturer



Sabre Autonomous Solutions

291 Milperra Road
Sydney, 2212 Australia
Contact: Damian Williams
Phone: 61-2-9792-2733
damian@sabreaautonomous.com.au
www.sabreaautonomous.com.au
Manufacturer

SAFE Systems, Inc.

18420 68th Ave S., #202
Kent, WA 98032
Contact: Glenn Seaverns
Phone: 425-251-8662
info@safesys.com
www.safesys.com
Manufacturer / Rental Company

Safespan Platform Systems, Inc.

252 Fillmore Avenue
Tonawanda, NY 14150
Contact: David Malcolm
Phone: 800-368-4010
dmalcolm@safespan.com
www.safespan.com
Manufacturer / Distributor / Rental Company

Safety Lamp of Houston

1816 Rotary Drive
Humble, TX 77338
Contact: Jim Reeves
Phone: 281-964-1019
sales@safetylampofhouston.com
www.safetylampofhouston.com
Distributor

Scangrit

Eastfield Road South Killingholme
Immingham, DN40 3NF United Kingdom
Contact: Gerry Bourke
Phone: 44-1469-574715
sales@scangrit.co.uk
www.scangrit.co.uk
Manufacturer / Distributor

Sea to Sky Innovations Ltd

Unit 204, 6741 Cariboo Road
Burnaby, BC V3N 4A3 Canada
Contact: Graham Sims
Phone: 604-420-7707
gsims@socomore.com
www.sea2skyglobal.com
Manufacturer

SEMicro Div., M.E. Taylor Engr. Inc.

15817 Crabbs Branch Way
Rockville, MD 20855
Contact: Kellie Taylor
Phone: 301-975-9798
sales@semicro.org
www.adhesiontesting.com
Manufacturer / Rental Company

Seminole Equipment, Inc.

204 Tarpon Industrial Circle
Tarpon Springs, FL 34689
Contact: Jim Klimis
Phone: 727-944-4481
jim3ds@hotmail.com

Seoul Shot Industry Co., Ltd - South Korea

58-1 Seongju-dong Seongsan-gu
Changwon, 641120 South Korea
Contact: Customer Service
Phone: 82-55-283-3735
contact.south-korea@wabrasives.com
Manufacturer

Equipment Company Profiles

Seymour Midwest LLC

PO Box 1674
Warsaw, IN 46581
Contact: Ryan Miller
Phone: 800-815-7253
ryan.miller@seymour.midwest.com
www.seymourmidwest.com
Manufacturer

Shanghai Shengchang Industry Equipment Co., Ltd.

#58, Lane 7224, Hunan Rd., Pudong
Shanghai, 201314 China
Contact: Jinyan
Phone: 86-21-58204865
info@ssce.cn
www.ssce.cn
Manufacturer

Shur-Line

4051 South Iowa Ave
St. Francis, WI 53235
Contact: Amy Kansaku
Phone: 800-253-7856
shurline.customerservice@shurline.com
www.shurline.com
Manufacturer

Siam IKK Co. Ltd - Thailand

416 Bangpoo Industrial Estate Moo 4 Sukhumvit Rd
Samutprakan, 10270 Thailand
Contact: Customer Service
Phone: 66-27-05-71-00
Manufacturer

SIBELCO / Eurogrit BV

Noordhoek 7
Papendrecht, 3351 LD Netherlands
Contact: Jeroen Keswiel
Phone: 31-78-6546770
abrasives@sibelco.com
www.eurogrit.com
Manufacturer / Distributor

SIE Industrial Ltd.

Faraday House, Station Rd,
Washington
Tyne & Wear, NE38 7LW United Kingdom
Contact: Gareth Bowen
Phone: 44-191-416-5127
info@sie-industrial.co.uk
www.sieindustrial.co.uk
Manufacturer / Distributor / Rental Company

Sierra Machinery, Inc.

939 Hawkins Blvd.
El Paso, TX 79915
Contact: Charlie Ward
Phone: 915-772-0613
www.sierraelpaso.com
Distributor

SJS Equipment LLC

101 Industrial Park Drive
Arma, KS 66712
Contact: Sheldon Bicknell
Phone: 620-347-8860
sheldon@sjsinc.net
www.sjsinc.net
Manufacturer

Sky Climber, LLC

1800 Pittsburgh Drive
Delaware, OH 43015
Contact: Todd King
Phone: 740-203-3931
info@skyclimber.com
www.skyclimber.com

Solvent Kleene, Inc.

119 Foster St. Bldg. #6
Peabody, MA 01960
Contact: Bob Sprei
Phone: 978-531-2279
sales@solventkleene.com
www.solventkleene.com
Manufacturer

Solvent Waste Management, Inc.

8103 Spring Cypress
Spring, TX 77379
Contact: Bill Palamountain
Phone: 281-379-3666
swm@solventwasher.com
www.solventwasher.com
Manufacturer

Southern Equipment Distribution, LLC

356 EMS Tower Road
Woodbine, GA 31569
Contact: Shannon Reifsnnyder
Phone: 912-882-7803
sesdistribution@tds.net
www.southernequipment-distribution.com
Distributor

Southern Industrial Supply, Inc.

4216 Westcap Rd
Whites Creek, TN 37189
Contact: Steven Wadsworth
Phone: 800-202-3820
office@southern-industrial.com
www.southern-industrial.com
Distributor / Rental Company

Specialty Products, Inc. (SPI)

2410 104th St. Ct. S., Suite D
Lakewood, WA 98499
Contact: Chas Weatherford
Phone: 253-588-7101
info@specialty-products.com
www.specialty-products.com
Manufacturer

Specialty Vacuum Inc.

4533 Green Park Road
St. Louis, MO 63123
Contact: Noel Prudent
Phone: 800-448-2801
vacitall@aol.com
www.specialtyvacuum.com
Rental Company

Spider By BrandSafway

365 Upland Dr.
Seattle, WA 98188
Contact: Spider
Phone: 877-774-3370
spider@spiderstaging.com
www.spiderstaging.com

Spin Import Export

Calea Ferentari Nr 135
Bucuresti, 51857 Romania
Contact: 40-722258552
Phone: 40-214561226
office@pardoseli-industriale.com
www.sisteme-industriale.ro
Distributor

Sponge-Jet, Inc.

14 Patterson Lane
Newington, NH 03801
Contact: Michael Merritt
Phone: 603-361-7950
sjadmin@spongejet.com
www.spongejet.com
Manufacturer

Spraytech, Inc., Global Spray Solutions

15179 West Hwy. 54
Wichita, KS 67235
Contact: Dave Calvin
Phone: 316-943-3700
dcalvin@globalspray.com
www.globalspray.com
Manufacturer

Starblast - by Chemours

5222 Treat Road
Starke, FL 32091
Contact: Jessica Stacy
Phone: 904-964-1326
jessica.stacy@chemours.com
www.chemoursabrasives.com
Manufacturer

Stone Tucker Instruments Inc.

51 Scott Street West
St. Catharines, ON L2R 1E2 Canada
Contact: Tyler Heywood
Phone: 905-688-5800
info@stone-tucker.com
www.stone-tucker.com
Distributor

Strategic Materials Inc.

17220 Katy Freeway
Houston, TX 77094
Contact: Sales
Phone: 281-647-2700
abrasives@strategicmaterials.com
www.trueabrasives.com
Manufacturer

Sulzer Mixpac USA Inc.

8181 Coleman Road
Haslett, MI 48840
Contact: Kari Holcomb
Phone: 800-822-8114
ct_sms_ame_sales_hs@sulzer.com
www.cox-applicators.com
Manufacturer

Sunnyside Corporation/Back To Nature Products

225 Carpenter Avenue
Wheeling, IL 60090
Contact: Adam Newman
Phone: 847-541-5700
anewman@sunnysidecorp.com
www.sunnysidecorp.com
Manufacturer

Surface Jet Inc.

PO Box 9747
New Iberia, LA 70562
Contact: Jeff Cole
Phone: 504-491-1329

Surface Prep Supply

#2 US Hwy. 17-92 North
Haines City, FL 33844
Contact: Derek Newberry
Phone: 863-419-9673
dnewberry@prepsupply.com
www.prepsupply.com
Manufacturer / Distributor / Rental Company

Surface Preparation-Texas, LLC

5973 South Loop East
Houston, TX 77033
Contact: Customer Service
Phone: 800-374-4043
info@surfacepreparation.com
www.surfacepreparation.com
Distributor

Equipment Company Profiles

SURFACE Worldwide, LLC

561 Keystone Avenue #317
Reno, NV 89503

Contact: Ron Benson

Phone: 612-338-1377

info@surfaceprep.com

www.surfaceprep.com

Manufacturer

The TDJ Group, Inc.

18-6 E. Dundee Rd., Suite 100
Barrington, IL 60010

Contact: James Lively

Phone: 800-252-7869

tdj@blastox.com

www.blastox.com/

Manufacturer

Techni-Quip Inc.

256 Wanaque Ave., Ste. 201
Pompton Lakes, NJ 07442

Contact: Paul Hellenen

Phone: 973-835-6500

blastgrit@gmail.com

blastgrit.com

Distributor

Temco Distributors

3 Forge Street
Welshpool, 6106 Australia

Phone: 61-8-9350-5940

sales@temco.com.au

temco.com.au

Distributor

Tennant Coatings

2454 Louisiana Av N
Golden Valley, MN 55427

Contact: Coatings Sales

Phone: 800-540-1299

www.tennantcoatings.com

Manufacturer

Testex

303 Markus Court
Newark, DE 19713

Contact: Mary Ellen Stachnik

Phone: 302-731-5693

mestachnik@testextape.com

www.testextape.com

Manufacturer

Texan Stone LLC

11806 Wilcrest Drive, Suite 202
Houston, TX 77031

Contact: Mani Palani

mani@texanstone.com

www.texanstone.com

Distributor

Thermion

PO Box 780
Silverdale, WA 98383

Contact: Dean Hooks

Phone: 360-692-6469

dhooks@thermioninc.com

www.thermioninc.com

Manufacturer

Thomas Abrasives (Pty), Ltd - South Africa

29 Smits Street
Germiston, Gauteng Province, 1401
South Africa

Contact: Customer Service

Phone: 27-11-821-2813

contact.south-africa@wabrasives.com

www.wabrasives.com

Manufacturer

Tioga HVAC Rentals & Sales

4810 Lilac Drive North
Minneapolis, MN 55429

Contact: Greg Gundrum

Phone: 763-525-4000

ggundrum@tiogaairheaters.com

www.tiogaairheaters.com

Manufacturer / Rental Company

Titán Tool

1770 Fernbrook Lane
Minneapolis, MN 55447

Contact: Kevin Coleman

Phone: 229-726-6823

colemank@titantool.com

www.titantool.com

Manufacturer / Distributor / Rental Company

TMS Metalizing Systems, Ltd.

7765 NW Eldorado Blvd #101
Bremerton, WA 98312

Contact: Dave Wixson

Phone: 360-692-6656

info@tmsmetalizing.com

www.tmsmetalizing.com

Manufacturer / Distributor / Rental Company

Total Enclosure Sail System, Inc.

7106 Northaven Dr.
Dallas, TX 75230

Contact: Bret Walton

Phone: 800-724-5710

bret@sailsystem.com

www.sailsystem.com

Manufacturer / Distributor / Rental Company

Tower Sealants / M-D Building

2095 Memorial Park Rd.
Gainesville, GA 30504

Contact: Ray Heck

Phone: 405-557-3557

heckr@mdteam.com

www.towersealants.com

Manufacturer

TQC Sheen

Molenbaan 19
Capelle aan den IJssel, 2908LL
Netherlands

Contact: Esther Krijgsman

Phone: 31-10-7900100

info@tqcsheen.com

www.tqcsheen.com

Manufacturer / Distributor

TQC Sheen USA

3689 Hadley Road
Metamora, MI 48455

Contact: Joel Bialek

Phone: 810-678-2400

joel@tqc-usa.com

www.tqc-usa.com

Manufacturer / Distributor

Tractel Inc.

51 Morgan Dr. Suite 1
Norwood, MA 02062

Contact: Sales department

Phone: 800-421-0246

tractel.usa-east@tractel.com

www.tractel.com

Manufacturer / Distributor

Tramex Meters

Unit F Glencormack Business Park
Kilmacanogue

County Wicklow, A98D9K3 Ireland

Contact: Sales Team

Phone: 800-234-5849

sales@tramexmeters.com

www.tramexmeters.com

Manufacturer

Trask-Decrow Machinery, Inc.

52 US Route 1 #2
Scarborough, ME 4074

Contact: Mark Callahan

Phone: 800-287-1538

mcallahan@tdmgo.com

www.getdryair.com

Distributor

Trelawny Surface Preparation Technology

13 Highdown Road, Sydenham
Industrial Estate

Warwickshire, Leamington Spa,
CV31 1XT United Kingdom

Contact: Kevin Sharrock

Phone: 44-1926-883781

sales@trelawny.co.uk

www.trelawny.co.uk

Manufacturer / Distributor

T

T Tex Industries LP

8302 Alameda Genoa
Houston, TX 77075

Contact: Darrell Todd

Phone: 800-367-7306

sales@ttexindustries.com

www.ttexindustries.com

Distributor

Target Products Ltd.

9503 87th Ave
Morinville, AB T8R 1K6 Canada

Contact: Neil Moore

Phone: 780-939-3033 or

800-575-0500

nmoore@targetproducts.com

www.targetproducts.com

Manufacturer / Distributor

Tarps Manufacturing, Inc.

1000 State Hwy 104
Meredosia, IL 62665

Contact: Rich Ott

Phone: 877-584-1900

irctom@ircgrp.com

www.tarpsmfg.com

Manufacturer

TCR Blast Abrasives

5737 West Park Ave.
St. Louis, MO 63110

Contact: Keith Gabbard

Phone: 314-241-5333

keith@tcrcoatings.com

www.blastabrasives.com

Distributor

Equipment Company Profiles

Trimaco, LLC

2300 Gateway Centre Blvd, Suite 200

Morrisville, NC 27560

Phone: 314-534-5005

customerservice@trimaco.com

www.trimaco.com

Manufacturer

Tritech Industries, Inc.

610 Rahway Avenue

Union, NJ 07083

Contact: Dan Hosley

Phone: 908-378-1080

dhosley@tritechindustries.com

www.tritechindustries.com

Manufacturer

TriVistro Corporation

150 Nickerson Street Suite 107

Seattle, WA 98109

Contact: Jeff Freas

Phone: 888-301-0181

info@trivistro.com

www.glassabrasive.com

Manufacturer

Tronox

1735 Market Street

Philadelphia, PA 19103

Contact: Linda Conners

Phone: 215-845-4536

linda.conners@tronox.com

alkali.tronox.com

Manufacturer

TST Sweden, AB

Prastgatan 12

SE-511 54 Kinna, Sweden

Contact: Peder Lindstrom

Phone: 46-320-20-58-72

peder@tst-sweden.se

www.tst-sweden.com

Manufacturer

Turtle Creek Software

119 S Cayuga St #304

Ithaca, NY 14850

Contact: Casey McD

Phone: 607-220-4514

info@turtlesoft.com

www.turtlesoft.com

Manufacturer



U.S. Metals, Inc.

3180 S State Road 19

Mentone, IN 46539

Contact: James L Green II

Phone: 800-433-6244

usmetals@comcast.net

www.usmetalsinc.com

Manufacturer

Unified Technologies

3015 Center Dr.

Cleveland, OH 44134

Contact: Art Koch

Phone: 440-897-5226

artkoch123@gmail.com

www.ut-unifiedtechnologies.com

Distributor

Unimanix

2205 Chemin St-Francois

Dorval, QC H9P 1K3 Canada

Contact: Nazareth Tankarian

Phone: 514-550-0809

nt@unimanix.com

www.unimanix.com

Manufacturer

Uni-Ram Corporation

381 Bentley St.

Markham, ON L3R 9T2 Canada

Contact: Jay Farquharson

Phone: 800-417-9133

jay@uniram.com

www.uniram.com

Manufacturer

Uni-Royal Pack Co., Ltd.

3, Soi Pattanakarn 50, Pattanakarn Rd.

Suanluang, Bangkok, 10250

Thailand

Contact: Tanasit Asawakanoksilp

Phone: 66-2-720-4400

urpgroup@truemail.co.th

www.uniroyalpack.com

Distributor

United Abrasive, Inc.

N1534 Sturgeon Mill Road;

PO Box 98

Vulcan, MI 49892

Contact: Bill Paupore or Becky

Langin

Phone: 800-228-2925

uainc@uplogon.com

Manufacturer / Distributor

Universal Acoustic & Emission Technologies, Inc.

Avenida Mantenimiento No. 130

San Luis Potosi, 78395 Mexico

Contact: Antonio Duran

Phone: 52-444-870-47-00

aduran@universalaet.com

http://www.universalaet.com

Manufacturer

URACA GmbH & Co. KG

Sirchinger Str. 15

Bad Urach, 72574 Germany

Contact: Herbert Queiser

Phone: 49-7125-133-0

h.queiser@uraca.de

www.uraca.de

Manufacturer

US Minerals

18635 West Creek Drive

Tinley Park, IL 60477

Contact: Jason Vukas

Phone: 708-623-1943

jvukas@us-minerals.com

www.blackdiamondabrasives.com

Manufacturer / Distributor



Van Air Systems

2950 Mechanic St.

Lake City, PA 16423

Contact: Sales

Phone: 800-840-9906

info@vanairsystems.com

www.vanairsystems.com

Manufacturer

Vector Technologies Ltd.

8301 W. Parkland Court

Milwaukee, WI 53223

Contact: David Mitchell

Phone: 800-832-4010

inquiry@vector-vacuums.com

www.vector-vacuums.com

Manufacturer

Victory Air & Equipment, Inc.

P O Box 3584

Victoria, TX 77903

Contact: Danny Hanselman

Phone: 361-573-0819

dhanselman@victory-air.net

victory-air.net

Distributor

VitaFlex USA

1305 Graham Street

Burlington, NC 27216

Contact: Flora Lin

Phone: 888-616-9948

sales@vitaflexusa.com

www.vitaflexUSAstore.com

Manufacturer

VLN Advanced Technologies Inc.

1166 Rainbow Street

Ottawa, ON K1J 6X7 Canada

Contact: Willie Bloom

Phone: 613-747-0107

wbloom@vln-tech.com

www.vln-tech.com

Manufacturer

VR Coatings Pvt. Ltd.

J-138, Bhosari Industrial Area,

MIDC Bhosari

Pune, 411026 India

Contact: Mr. A A Dighe

Phone: 91-20-27130331

sales@vrcoatings.com

www.vrcoatings.com

Manufacturer

Vulkan Blast Shot Technology

10 Plant Farm Blvd., Unit 2

Brantford, ON N3S 7W3 Canada

Contact: Customer Service

Phone: 800-263-7674

vulkan@vulkanshot.com

www.vulkanshot.com

Manufacturer / Distributor



W Abrasives

1 Abrasive Avenue

Bedford, VA 24523

Contact: Michael Cagnoli

Phone: 800-207-4691

contact.united-states@wabrasives.com

com

www.wabrasives.com

Manufacturer

Equipment Company Profiles

WA Kurgan - Russia

12/1, 3 Floor, Office 303 Sibirsky
Trakt Street
Ekaterinburg, 620100 Russia
Contact: Customer Service
Phone: 7-352-265-35-05
contact.russia@wabrasives.com
www.wabrasives.com

The Warehouse Rentals and Supplies

1335 S. Main Street
Greensburg, PA 15601
Contact: Sales Department
Phone: 800-621-2777
sales@twrs.com
www.twrs.com
Manufacturer

Washington Air Compressor Rental Co.

1800 4TH Street, NE
Washington, DC 20002
Phone: 202-635-1500
Distributor

Washington Air Compressor Rental Co.

44180 Wade Dr.
Chantilly, VA 20152
Phone: 703-742-6200
Distributor

Washington Air Compressor Rental Co.

7304 Grove Road
Frederick, MD 21704
Phone: 301-662-7711
Distributor

Washington Air Compressor Rental Co.

12529 Parklawn Dr.
Rockville, MD 20852
Contact: Steve Cranford
Phone: 301-230-5800
Distributor

Water Canadianon

4300 W. Lake Mary Blvd Units
1010-424
Lake Mary, FL 32746
Contact: Mark Williams
Phone: 800-333-9274
sales@watercannon.com
www.watercannon.com
Distributor

Wegener Welding LLC

16W301 S. Frontage Rd.
Burr Ridge, IL 60527
Contact: Liz Turner
Phone: 630-789-0990
info@wegenerwelding.com
www.wegenerwelding.com
Distributor

WerkMaster Grinders & Sanders Inc.

1448 Charlotte Rd.
North Vancouver, BC V7J 1H2
Canada
Contact: Gord Siddall
Phone: 604-629-8700
Sales@werkmaster.com
www.werkmaster.com
Manufacturer

Westech

1002 15th Avenue
Nisku, AB T9E 7S5 Canada
Contact: sales@westechvac.com
Phone: 780-955-3030
sales@westechvac.com
www.westechvac.com
Manufacturer / Distributor

Winoa Canada Inc. - Canada

650 Rusholme Rd
Welland, ON L3B5N7 Canada
Contact: Customer Service
Phone: 800-207-4691
contact.canada@wabrasives.com
Manufacturer

Winoa China

Suite 1209-1210 Bldg 1 - City Center
166 Min Hong Rd
Shanghai, 201100 China
Contact: Customer Service
Phone: 86-21-5219-88-77
contact.china@wabrasives.com
Manufacturer

Winoa Deutschland

August-Schanz-Straaye 27b

Frankfurt, 60433 Germany

Contact: Customer Service
Phone: 49-0-76-66-93-26-813
contact.germany@wabrasives.com
www.wabrasives.com
Manufacturer

Winoa FRANCE

528 Avenue de Savoie
Le Cheylas, 38570 France
Contact: Customer Service
Phone: 33-0-4-76-92-92-61
contact.france@wabrasives.com
www.wabrasives.com
Manufacturer

Winoa Iberica SA - Spain (TFM)

Paseo de la Magdalena, 28
Balmaseda, 4800 Spain
Contact: Customer Service
Phone: 34-94-68-02-938
contact.spain@wabrasives.com
www.wabrasives.com
Manufacturer

Winoa Mexico

105 Av. Las Palmas
Monterrey, 66368 Mexico
Contact: Customer Service
Phone: 52-818-032-8318
contact.mexico@wabrasives.com
www.wabrasives.com
Manufacturer

Winoa Middle East & Africa

P.O. Box 293586 Bldg. 4W-Block A,
Office 508
Dubai, United Arab Emirates
Contact: Customer Service
Phone: 971-4-295-2241
contact.uae@wabrasives.com
www.wabrasives.com
Manufacturer

WIWA LLC

107 N. Main street
Alger, OH 45812
Contact: Caleb Meacham
Phone: 567-674-1907
sales@wiwalp.com
www.wiwausa.com
Manufacturer

The Wooster Brush Company

604 Madison Ave., PO Box 6010
Wooster, OH 44691
Contact: Mary Stark
Phone: 800-392-7246
customerservice@woosterbrush.com
www.woosterbrush.com
Manufacturer

Z

Zibra

172 Broad Sound Place
Mooresville, NC 28117
Contact: Mike Sherman
Phone: 704-271-4500
mikesherman@enjoyZibra.com
www.enjoyzibra.com
Manufacturer

Zip Wall Dust Barrier System

37 Broadway, #2
Arlington, MA 02472
Contact: Matt Hete
Phone: 302-344-8988
info@zipwall.com
Manufacturer

77 F & 50% RH

Cure times most often defaulted to in standard laboratory conditions.

See page 13.

2.5 hours

The recoat window, which was exceeded, causing adhesion problems between an anticorrosive coating and an antifouling coating on a ship's hull.

See page 9.

28

The number of wind power projects that the U.S. has in progress according to the U.S. Office of Energy Efficiency and Renewable Energy, totaling 23,735 MW of power.
See page 16.

70

Years since the founding of G.C. Zarnas & Co., Inc., in 1948 by former college football All-American Gust C. Zarnas.
See page 6.

31

The number of product categories listed in the annual *JPCL* Equipment Buying Guide.
See page 31.

0 to 2.5 feet per second

The increase in velocity between the rake arm and the water in a wastewater treatment clarifier that can double the corrosion rate of bare steel.
See page 21.